

GOLD MEDAL

WRITING TABLET

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THE GIRDLER CORPORATION
INCORPORATED
VOTATOR DIVISION
GENERAL OFFICES
LOUISVILLE 1, KENTUCKY

December 3, 1947.

A. Brothman and Associates,
Chemical and Mechanical Engineers,
85-03 — 57 Avenue,
Elmhurst, L.I.

Attention: Mr. A. Brothman, Chief Engineer.

Gentlemen:

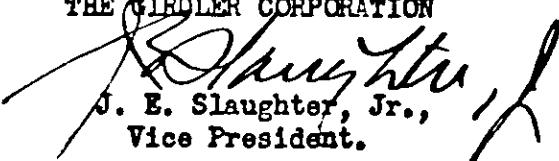
We have your request for literature on our Votator equipment and are pleased to enclose several circulars and pieces of literature describing the Votator principle of heat transfer and processing and illustrating several models of Votator units designed for different applications. At the present time our general catalog is in the process of revision but will not be issued for several months.

We are forwarding a copy of your letter to our Eastern Sales Manager, Mr. S. N. Welch, located at 150 Broadway, New York City. If, after reviewing the enclosed literature, you wish further particulars, please contact Mr. Welch at the above address.

Thanking you for your interest, we are

Very truly yours,

THE GIRDLER CORPORATION


J. E. Slaughter, Jr.,
Vice President.

JES/cla
encls.

Wherever liquid or viscous materials are processed, consider Votator!

The Votator and Processing Edible Oils

The Girdler Corporation, manufacturers of the VOTATOR, was the first to provide equipment for processing margarine continuously. Use of the VOTATOR completely changed the entire method of manufacture of margarine, with the result that Girdler is considered to have made the greatest single contribution to this industry's production efficiency. In the production of shortening and lard, the VOTATOR is used for chilling and plasticizing, and has also made these operations continuous and much more efficient. Today 75% of the nation's shortening and margarine, and a large and fast-growing percentage of its lard, are VOTATOR-made. In each application, the VOTATOR begins with the prepared hot oils (and other ingredients, if any) and completes the manufacture of the product, delivering it to fillers or molding apparatus.

In these edible oils applications, the VOTATOR has improved the quality, uniformity, texture and color of the product. Moisture condensation and contamination have been minimized. Keeping, creaming, mixing and cooking properties have all been improved, and a more efficient use has been made of everything needed in production — materials, refrigerant, manpower, floor space and power.

The Votator and Processing Foods

By means of the VOTATOR, ice cream production was put on a continuous basis. Chilling was accomplished in seconds, which made possible an improved texture of the ice cream and precisely controlled aeration. This application of the VOTATOR has led to numerous others in the chilling of food products, and in all of these uses the above three advantages are of primary importance and outstanding as compared to other methods. The VOTATOR can also be used to cook food products in liquid, viscous or suspended form. Rapid removal of film by surface scraping permits higher temperatures without danger of burning or scorching. In all food processing, The VOTATOR'S closed operation, sanitary construction and easy cleaning are significant.

Other food applications include: *Fruit juices and purees* — quick chilling and crystallization. *Liquid whole eggs* — quick chilling and pasteurization. *Starch base solutions*, such as used in making salad dressings — continuous cooking and cooling.

The Votator and Processing Chemicals

The VOTATOR is suitable for processing a wide variety of chemicals that are in liquid or viscous form, at least during one stage of manufacture. The distinguishing feature of each of these applications is *uniform, continuous operation under controlled temperature* — continuous mixing, heating, cooling, emulsifying, plasticizing, etc. Of this broad group, the following are only typical:
Photographic emulsions — cooling and processing.
Textile printing gums — heating or cooling.
Leather preparations — cooling.
Liquid resins — continuous processing of resins . . . heating and cooling in fluid stage.
Waterproofing compounds — heating or cooling.
Gelatin and glue — heating or cooling.
Paper and textile coatings — uniform mixing with temperature control.
Wax Products — continuous cooling and emulsifying.
Shaving Creams — Chilling and Plasticizing.

The Votator and Processing Petroleum Products

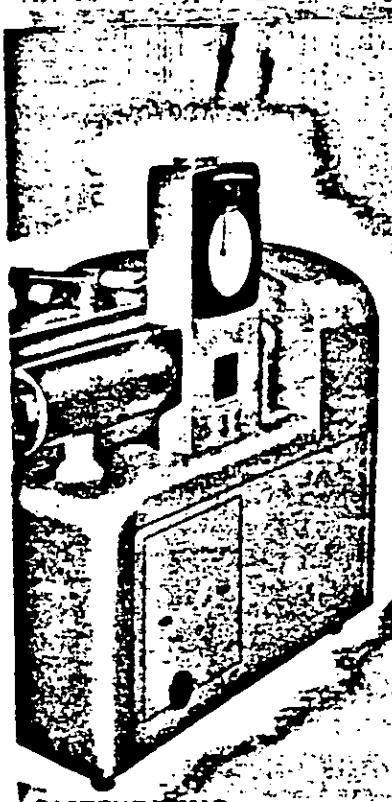
Use of the VOTATOR by the petroleum industry has led to various production short-cuts and new standards of quality, efficiency and safety. The following applications are typical and considerable information, including some pilot plant and plant data, is available:

Grease. A processing system for continuous production of lubricating greases.

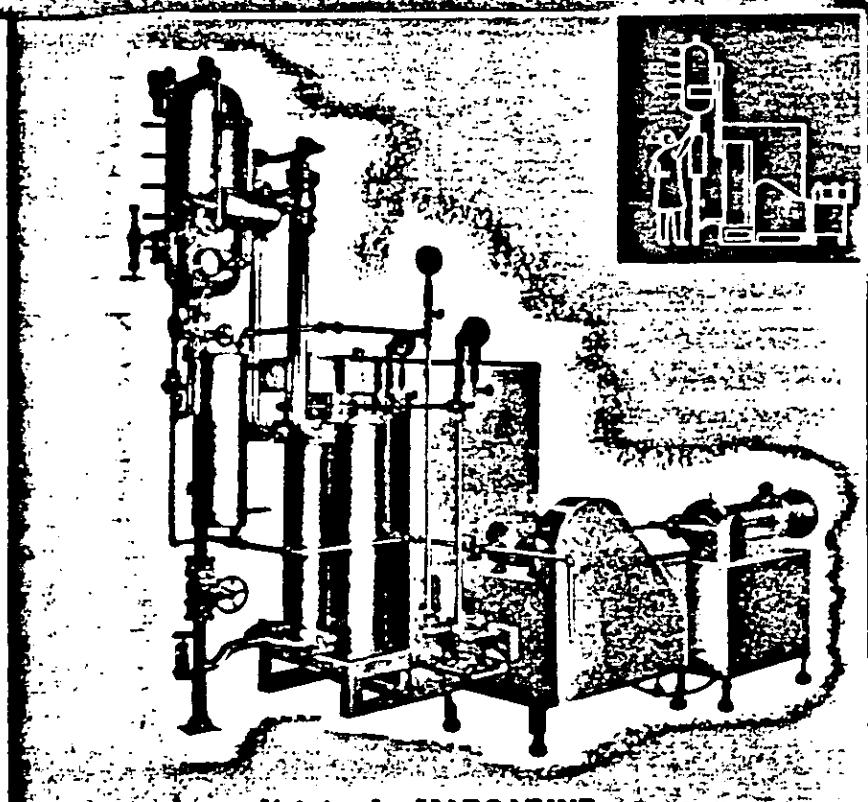
Wax. The VOTATOR is an efficient instrument for continuous crystallization and filling of paraffin wax.

Hydrocarbons. Very effective for low temperature crystallization of various hydrocarbons.

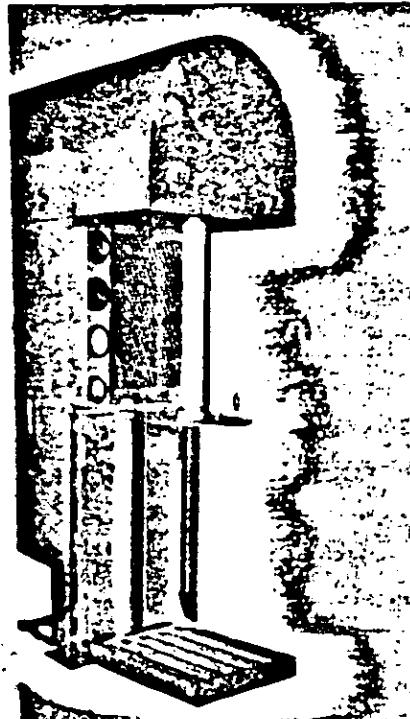
Alkylation. A special adaptation, called the VOTATOR Reactor, gives higher yield, higher octane and greater 3-C values in the production of aviation gasoline alkylate.



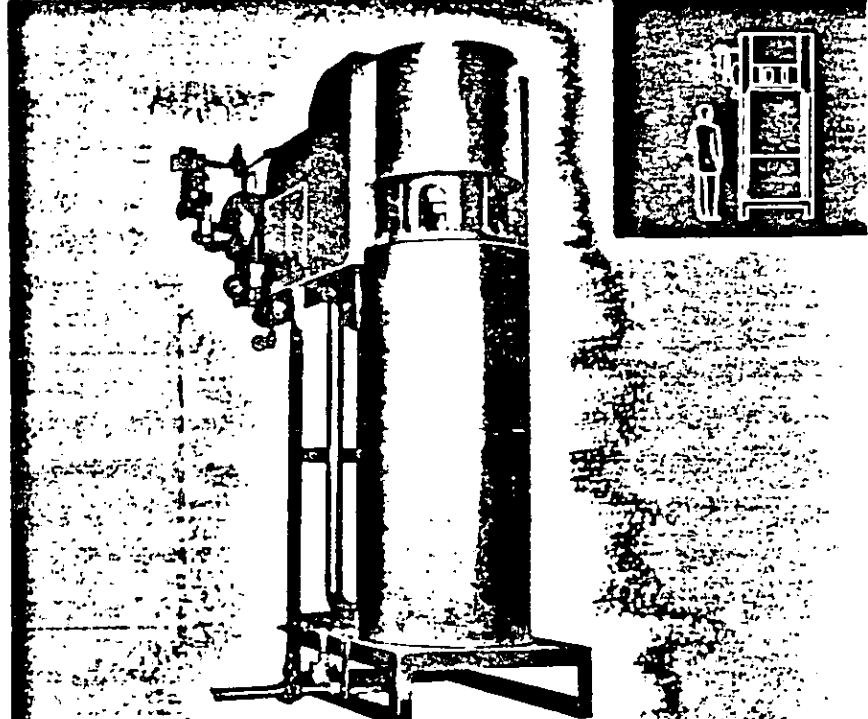
PASTEURIZING



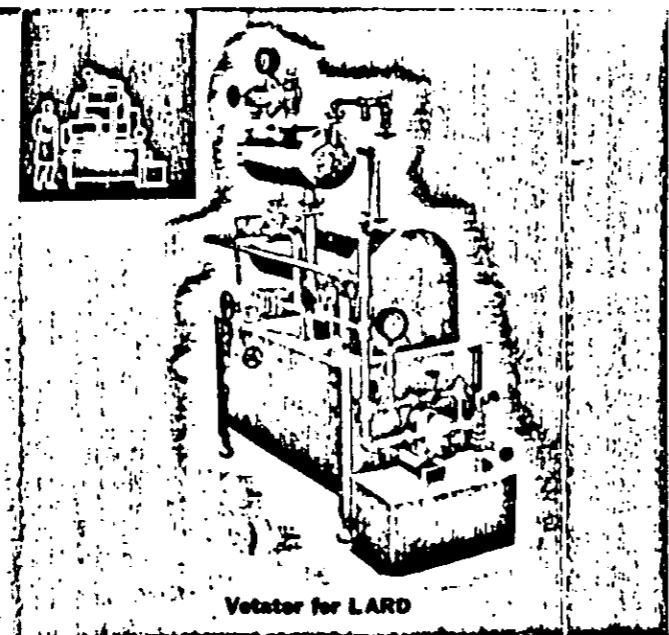
Votator for MARGARINE



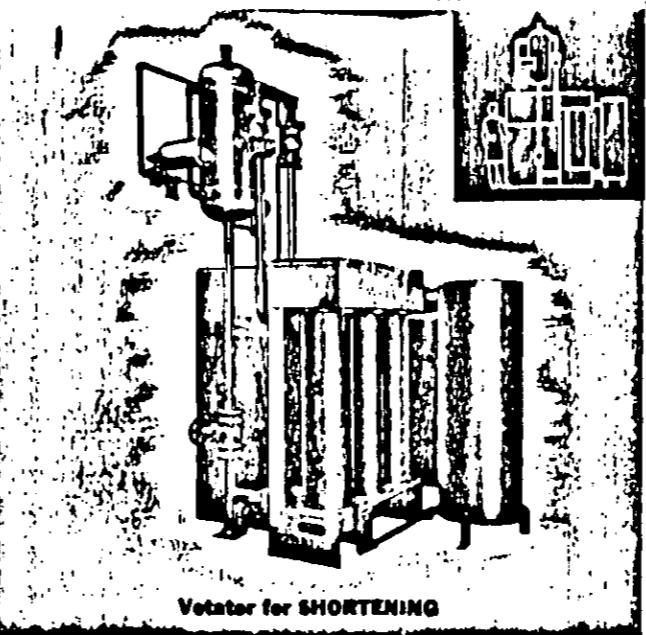
PARAFFINE WAX



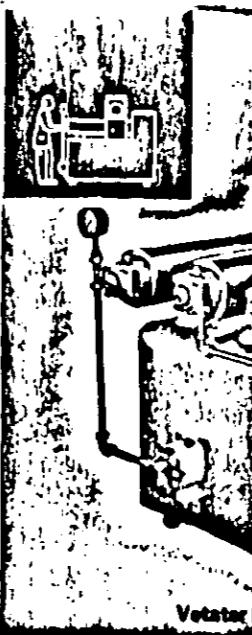
Votator for PROCESSING CHEMICALS



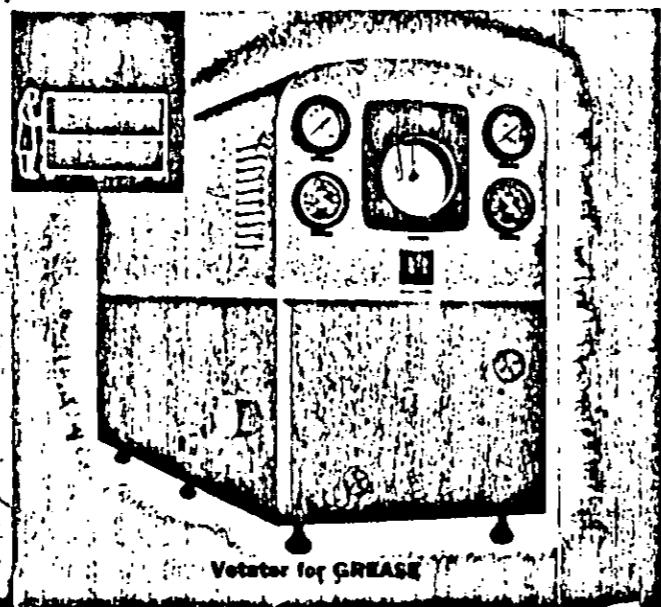
Votator for LARD



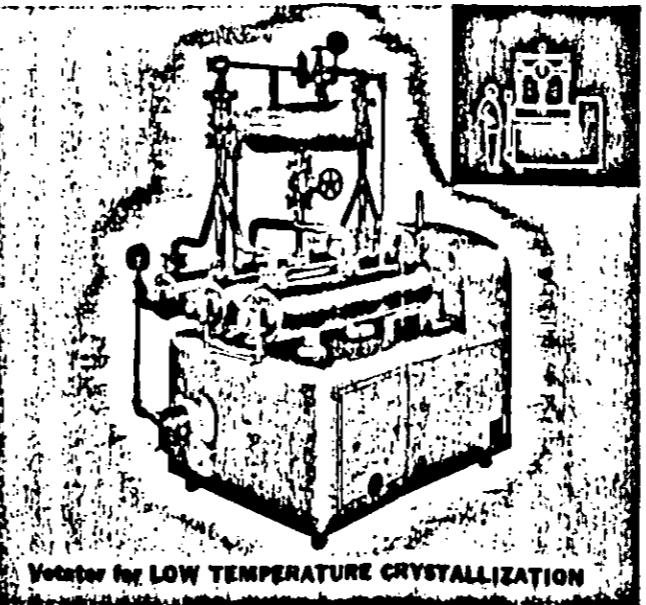
Votator for SHORTENING



Votator for CREAM



Votator for GREASE



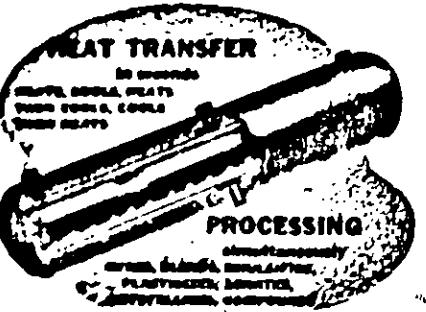
Votator for LOW TEMPERATURE CRYSTALLIZATION



Votator for FATS

Votator

CONTROLS UNIFORMITY AND
PRODUCTION EFFICIENCY
IN MANY INDUSTRIES!



THE VOTATOR processes virtually any liquid or viscous material, including the heavier viscous substances and those that tend to adhere to heat transfer surfaces or are otherwise difficult to handle with conventional equipment. For this reason and also because the continuous, closed, controlled operation insures the quality of the finished product, its application is being rapidly extended into new fields. The VOTATOR has had successful applications in heating the product to over 400°F and cooling the product to -30°F.

VOTATORS are built in a wide range of sizes to meet either large or small capacity requirements. VOTATOR equipment can be furnished in either carbon steel or special corrosion-resisting materials. Specific data on particular applications available on request.

TYPICAL
Votator
UNITS

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JWJ

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HEAT TRANSFER in the VOTATOR

Overall coefficients of 500 to 1150 B.t.u./hour) (square foot) ($^{\circ}$ F.) are easily obtainable on water-to-water heat interchange using the Votator. High agitation combined with scraping of the heat transfer wall produces thin films and high turbulence. The result is high rates of heat transfer even though the linear velocity through the Votator is less than 0.1 foot per second. This internal design leads to small size equipment which, in turn, allows high jacket velocities with low pressure drops. The Dittus-Boelter equation is used to calculate film coefficients on the jacket side where the flow is helical. The coefficients thus obtained check the experimental results within 10%. Film coefficients on the Votator side are found to increase less rapidly above a blade peripheral velocity of 13 feet per second for waterlike materials in the particular Votator design used.

THE Votator has been used extensively for processing margarine, shortening, and lard, because crystallization, plasticization, emulsification, and heat transfer may be brought about simultaneously. Its main accomplishment is processing, so that little stress has been put on the high heat transfer efficiency of the Votator. This paper deals with a water-to-water heat interchange test in which blade velocity, jacket-water velocity, and throughput rates were studied in relation to the over-all and film heat transfer coefficients.

A laboratory Votator, 8 inches in diameter and equipped with a 2.25-inch diameter shaft and two stainless steel blades, was designed for use with both water and ammonia. For water a sleeve insert cuts the height of the annular space to $\frac{1}{4}$ inch, and a baffle seal at one end prevents bypassing the water flow through the ammonia section. Copper tubing ($\frac{1}{4}$ -inch diameter) inside

the sleeve forms a helical water path around the nickel Votator tube. This method is apparently satisfactory since the heat balance—i.e., the quantity of heat flowing as measured from the jacket and Votator sides—checked to less than 2% for most cases. The assembly of this unit is shown in Figure 1.

The method consisted in pumping hot water (175° F.) at about 560 pounds per hour through the Votator and cooling it with a countercurrent flow of cold water (60° F.) on the jacket. Speeds of the mutator (a shaft with blades) were 200, 400, 800, 700, 1000, and 1900 r.p.m. Jacket-water velocities of 4.7, 5.1, 6.5, 7.5, 9.2, 12.9, 18.1, and 25.9 feet per second were tried. These corresponded to pressure drops through the jacket of 0.5, 1, 2, 3, 5, 10, 20, and 40 pounds per square inch. In two cases, 1900 and 400 r.p.m., the throughput rate was changed from 560 to 340 and 1800 pounds per hour, respectively. In all cases calibrated thermometers (0.2° F. subdivisions) were used, and the water rates were determined with a stop watch and scale tank. Thirty pounds of rotated water and 88 pounds of jacket water were weighed. Check readings were made to ensure that the equipment had come to equilibrium. The mutator speed was less accurate since the speed indicator could not be reliably read better than ± 10 r.p.m.

Three points should be considered for accurate analysis of the data—errors due to (a) movement in stagnant layer of water outside the sleeve insert, (b) any flow by-passing from one helical turn to the next, and (c) expansion and contraction losses at entrance and exit of jacket. This work neglects these errors since they are small and are apparently within the accuracy of the data—namely, 2%.

Agitation and Mixing

HEAT BALANCE

The quantity of heat flowing per hour was determined by multiplying the average specific heat by the weight rate of water flow and the temperature change of the water. This change in heat content of water flowing through the Votator and jacket were separately calculated; values checked in most cases to less than 2%. The correction for average specific heat was found unnecessary with the present accuracy.

Table I summarizes the data. Figure 2, constructed from the data of Table I, shows how the quantity of heat flowing, Q , varied with changes in mutator speed for several jacket-water (jw) velocities. It illustrates that the amount of heat flowing through the 0.7 square foot of cooling surface reached as high as 52,000 B.t.u. per hour, with 37,000 B.t.u. as about the average flow. Increased mutator speed increased the heat flow considerably, but the increase at the higher mutator speeds was much smaller, as shown by the following data taken at a jacket-water velocity of 9.8 feet per second ($\Delta P = 5$ pounds per square inch, 2900 pounds per hour):

Mutator Speed, R.P.M.	B.T.U. Removed per Hour	Mutator Speed, R.P.M.	B.T.U. Removed per Hour
300	22,750	700	37,000
500	34,500	1000	33,800

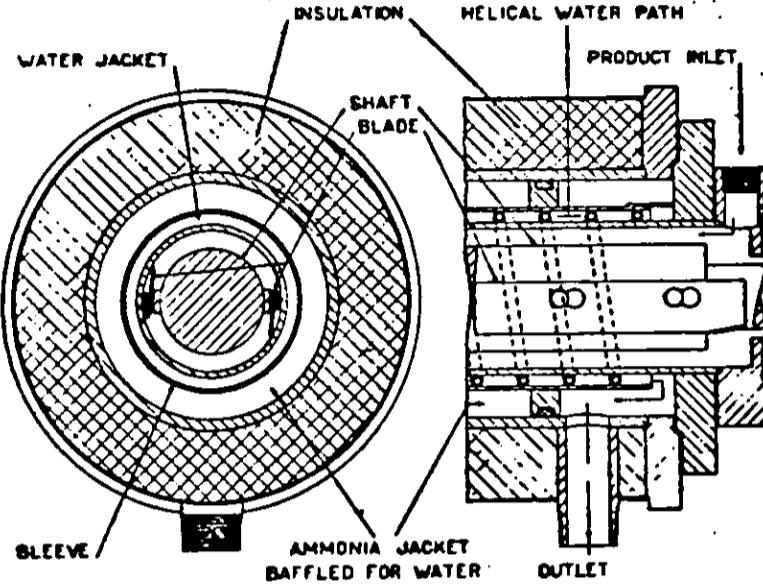


Figure 1. Longitudinal and Cross-Sectional View of Ammonia-Jacketed Laboratory Votator Baffled for Water

In going from 300 to 500 r.p.m., 2050 B.t.u. per hour more could be removed; in going from 700 to 1000 r.p.m., the increase was less than half as much, 1000 B.t.u. per hour. Obviously there should be a selection of the highest mutator speed which is consistent with power load, tube, blade, and bearing wear.

Black dots in Figure 2 indicate the few cases where the heat balance did not check closely. For this reason the values obtained from the rotated water side were used where the data were more reliable, since low rates and large temperature differences existed. By this procedure the curves became consistent with one another throughout all this work. Other points on the graph are an average of the data obtained from the jacket and Votator sides.

The bottom curve at a jacket-water velocity of 5 feet per second is smooth, but all other curves show a sharp break at 500 r.p.m. Also, the greatest increase in heat transfer for jacket-water velocities, 9 feet per second and above, occurred in going from 500 to 700 r.p.m.; at 5 feet per second the sharpest increase occurred at 300 to 500 r.p.m. The facts are explained later where it is more clearly shown that full turbulence apparently does not occur until a jacket-water velocity of 7.5 feet per second is obtained.

Table I. Data for Water-to-Water Heat Transfer

Temperature, ° F.						Rate, Lb./Hr.	Heat, B.T.U./Hr.	AP.	Q
Vol. min.	Jacket min.	Vot. min.	Jacket in.	LMTD	Vot. min.	Jacket	Vol. min.	Jacket	
300 Revolutions per Minute									
179.3	67.3	118.1	63.8	78.31	584.6	8158	27,410°	24,850	60
179.3	69.0	116.1	63.8	77.94	584.3	8113	26,320°	24,740	50
179.0	71.5	119.2	63.8	78.21	581.7	8093	24,740	24,690	10
179.3	74.0	122.7	63.8	80.45	577.1	2600	22,750°	22,320	5
179.3	76.3	124.8	63.0	80.62	582.8	2592	21,730	20,420	2
179.0	80.0	128.7	64.7	80.23	581.4	1802	20,340	20,430	1
400 Revolutions per Minute									
179.3	71.9	148.9	63.7	86.41	1780	5849	84,430	81,900	50
179.3	69.6	111.4	63.8	74.35	582.1	5804	28,580	27,990	50
179.3	81.0	126.0	63.0	78.93	581.5	1617	20,810	20,500	1
500 Revolutions per Minute									
179.4	68.8	103.1	63.8	67.83	585.8	8042	40,640	40,160	60
179.6	70.5	106.2	63.8	69.44	585.9	5721	29,320	28,280	70
179.4	72.8	110.0	63.8	71.00	583.3	4060	26,690	26,490	10
177.3	75.6	114.3	63.8	78.06	585.3	2192	24,990	24,760	5
177.3	77.4	116.4	64.0	73.55	582.3	2457	23,650	23,570	2
177.3	79.9	119.2	64.0	74.22	585.3	2039	22,170	22,360	2
177.7	83.3	121.0	64.3	78.01	589.8	1712	21,360	20,780	1
700 Revolutions per Minute									
179.4	69.1	100.8	63.0	67.83	586.8	8006	44,630°	41,940	60
179.0	70.1	103.4	63.8	68.82	582.3	5780	41,580	42,070	50
178.8	72.8	106.9	63.8	69.92	585.3	4060	29,450	29,320	10
179.0	76.0	112.2	63.8	72.53	585.9	2274	27,760	27,570	5
178.3	72.8	114.5	63.0	73.21	580.3	2215	25,430	25,250	2
178.4	83.0	120.2	63.1	74.58	589.3	1624	22,520	22,250	1
177.8	84.6	121.6	63.8	74.87	586.8	1464	21,320	21,140	1/2
1000 Revolutions per Minute									
179.6	70.5	102.1	63.8	68.54	583.7	5846	44,410	43,110	50
179.4	73.0	105.6	63.8	70.03	585.3	4044	41,670	42,400	10
178.8	78.0	109.8	63.8	71.41	583.8	2068	38,540	39,710	5
178.3	78.6	113.8	63.8	73.74	589.4	2329	36,970	37,200	2
178.6	84.1	119.7	63.7	76.15	586.8	1569	33,380	33,800	1
1200 Revolutions per Minute									
178.8	63.7	80.6	66.8	66.08	586.8	7426	51,640	51,630	60
177.6	65.6	83.3	66.6	67.43	581.7	5347	48,060	48,090	50
178.6	69.1	100.0	66.7	70.54	582.4	3623	42,020	49,890	10
170.0	61.1	76.7	66.8	61.38	583.8	7506	31,400°	32,650	60
170.6	63.1	79.4	66.8	64.60	587.1	5413	30,640°	34,080	30
171.8	64.1	85.0	66.9	66.56	582.9	8662	30,580°	33,670	50
1300 Revolutions per Minute									
178.8	63.7	80.6	66.8	66.08	586.8	7426	51,640	51,630	60
177.6	65.6	83.3	66.6	67.43	581.7	5347	48,060	48,090	50
178.6	69.1	100.0	66.7	70.54	582.4	3623	42,020	49,890	10
170.0	61.1	76.7	66.8	61.38	583.8	7506	31,400°	32,650	60
170.6	63.1	79.4	66.8	64.60	587.1	5413	30,640°	34,080	30
171.8	64.1	85.0	66.9	66.56	582.9	8662	30,580°	33,670	50
1400 Revolutions per Minute									
178.8	63.7	80.6	66.8	66.08	586.8	7426	51,640	51,630	60
177.6	65.6	83.3	66.6	67.43	581.7	5347	48,060	48,090	50
178.6	69.1	100.0	66.7	70.54	582.4	3623	42,020	49,890	10
170.0	61.1	76.7	66.8	61.38	583.8	7506	31,400°	32,650	60
170.6	63.1	79.4	66.8	64.60	587.1	5413	30,640°	34,080	30
171.8	64.1	85.0	66.9	66.56	582.9	8662	30,580°	33,670	50

* Over-all coefficient, U based on heat

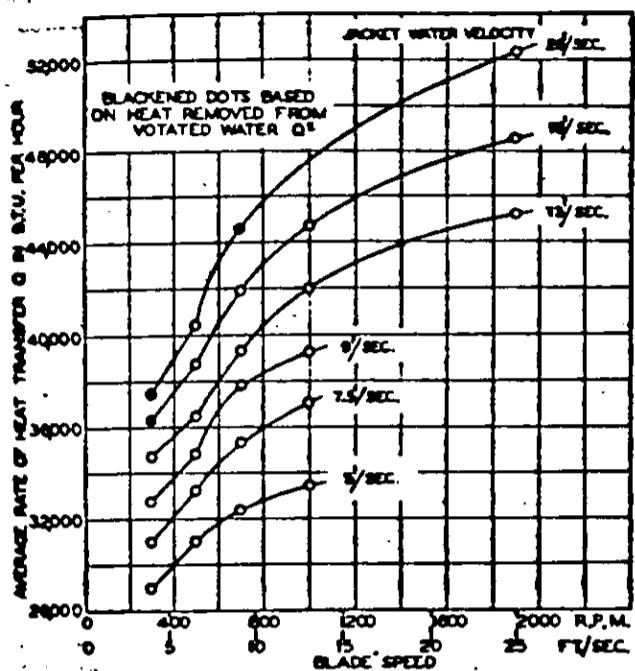


Figure 2. Effect of Blade Speed on Heat Transfer for Several Jacket Conditions

The data at 1900 r.p.m. do not fall on the 25, 18, and 15 foot per second lines. The correct velocities for these are 24, 17, and 11.6 feet per second; consequently, extrapolated values are included in Figure 2 to make the picture complete.

To simplify calculations on the jacket side, an over-all average was made of the average jacket temperatures obtained at various pressure drops. The inlet and outlet jacket-water temperatures were averaged for each Votator condition. Since these averages were quite close for different conditions on the Votator side, they were again averaged (Table II) in order to calculate the physical properties of the jacket water as given in Table III.

A plot of variation in transfer of heat with changes in jet velocities for the several mutator speeds showed that, up to 9 feet per second, the heat transfer increased linearly with increased velocity; above this value the increase tapered off. At a mutator speed of 700 r.p.m., 3700 more B.t.u. per hour were transferred in going from a jet velocity of 5 to 8 feet per second; in going from 20 to 23 feet per second, the increase was only 2100 B.t.u. per hour. Even the latter amount is considerable, so it is advisable to use the highest jet velocity possible and economical with the water pressure available.

Table III indicates that at 300-1000 r.p.m. a velocity of 25 feet per second required 8000 pounds of water flow per hour and a pressure drop of 40 pounds per square inch. Unless the water is to be used later at low pressure for further processing, these conditions are impractical without a booster pump. Values above 9 feet per second should be used in all possible installations where the amount of transferred heat increases at its maximum rate up to this point.

Table II. Inlet and Outlet Jacket-Water Averages

Mutator Pressure Drop, lb./sq. in.	Av. Jacket-Water Temp., °F.					Overall Av. Jacket Temp., °F.
	300 r.p.m.	400 r.p.m.	700 r.p.m.	1000 r.p.m.		
0.5	65.0	66.3	68.6	69.6	68.6	68.6
0.8	65.9	67.2	69.5	69.8	69.6	69.6
1.0	67.2	68.3	67.7	67.8	67.8	67.8
1.2	68.4	69.7	69.4	69.3	69.3	69.3
1.5	69.7	70.7	70.7	70.6	70.4	70.4
1.8	72.0	73.2	73.1	73.4	73.5	73.5
2.0	74.0	..	74.0	74.0

OVER-ALL COEFFICIENTS

The over-all coefficients were calculated from the average quantity of heat flowing, Q , by the following equation:

$$Q = UA_e LMTD \quad (1)$$

The amount of heat being transferred per hour, Q , is proportional to the cooling surface area, A_e , and the driving force, $LMTD$.

Cooling area A_e was 0.7 square foot of scraped surface for our unit. This figure was based on the assumption that the flanged heads of the jacket (Figure 1) were only half effective for cooling and that the cooling space occupied by the helical baffle was negligible. Certainly the cooling area will not be appreciably larger than this, and if the baffle does effectively occupy space, the calculated over-all coefficient, U , is on the conservative side. The over-all coefficients were calculated on the basis of effective scraped surface.

EFFECT OF MUTATOR SPEED. The effect of mutator speed in the range 300-1900 r.p.m. on over-all coefficient U is shown in Figure 3. In contrast to the heat quantity curves (Figure 2), these curves are smooth and do not show the pronounced break at 500 r.p.m. Here, as previously discussed, the points at 1900 r.p.m. are extrapolated values. The largest U obtained was about 1140 B.t.u./(hour)(square foot)(° F.), and the average was close to 800. The most rapid change in U occurred at the lower speeds.

The increase in U slowed down after 600 r.p.m. It would obviously be poor efficiency to operate below 600 r.p.m. for this liquids, and as discussed in the section on Heat Balance, it is advisable to use the highest mutator speed consistent with wear and power. The peripheral speed at 600 r.p.m. was 7.8 feet per second. As a result of the high over-all coefficient U obtained by scraping, the size of equipment is small, and high jacket-water velocities and film coefficients can be obtained with small pressure drops.

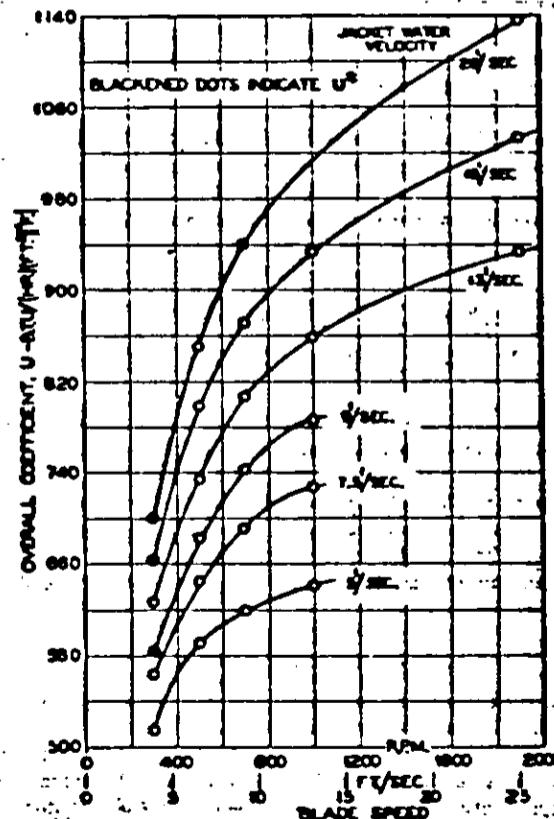


Figure 3. Effect of Blade Speed on Over-all Coefficient of Heat Transfer for Several Jacket Conditions

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Agitation and Mixing

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Table III. Jacket Average Data

(Annular space = 1.986×10^{-3} sq. ft., equivalent diameter $D_e = 0.0334$ ft.)

Pressure drop, lb./sq. in.	300-1000 R.P.M.				1900 R.P.M.			
	A.v. temp., °F.	A.v. rate, lb./hr.	lb./sq. ft./sec.	Density, lb./cu. ft.	Viscosity, centipoises	A.v. vol., sec.	Vol. vol., sec.	Pressure drop, lb./sq. in.
40	65.5	8096	1612	62.8	1.036	25.58	75,000	600
50	66.6	8664	1128	62.50	1.024	18.10	55,400	50
55	67.8	4038	804.3	62.28	1.012	13.91	38,500	30
60	69.2	2021	561.6	62.27	0.987	9.83	22,900	10
65	70.4	2247	467.8	62.26	0.972	7.51	22,900	6
70	71.8	3039	405.9	62.25	0.958	6.52	21,100	3
75	73.8	1501	316.8	62.24	0.943	5.09	17,000	1
80	76.0	1668	301.7	62.23	0.929	4.00	15,000	0.5

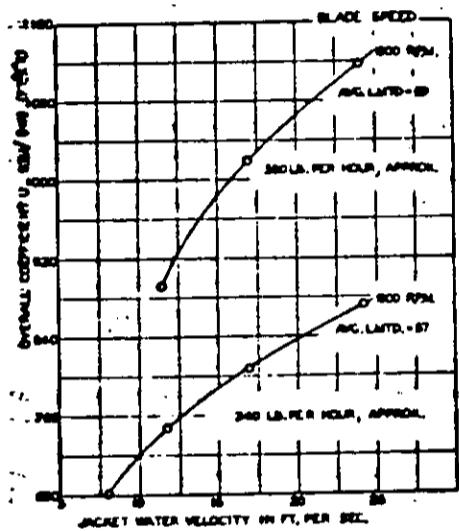


Figure 4. Effect of Changes in Rate and Temperature of Votator Water on Overall Coefficient

EFFECT OF CHANGES IN CONDITIONS ON VOTATOR SIDE. The rate of votated water was varied in two cases. At 1900 r.p.m. about 580 and 340 pounds per hour were tried at three jacket water velocities (Figure 4). At 400 r.p.m., rates of 1800 and 560 pounds were used. The data are given in Table I. Figure 4 shows the difference in over-all coefficient obtained. In addition to a change in throughput rate, the log mean temperature difference varied. The following data for 340 pounds per hour were based on the heat change of the votated water, Q_v , since the heat change of the jacket water, Q_j , was inconsistent and erratic:

LMTD	Rate, Lb./hr.	Mean Temp., °F.	Votator Speed, R.P.M.	Overall Coefficient, U	
				Q	U
22	570	60	1900	48,000	1018
22	340	50	1900	30,600	804

Since the jacket-water temperature and velocity were about equal, the film coefficient would be about the same in the two cases. Consequently, the change had to do with a difference in phenomena on the Votator side. The log mean temperature difference decreased about 20%. The heat load dropped about 36%, and the over-all coefficient was lowered about 20%. The log mean temperature difference is the main contributing factor, as would be expected.

FILM COEFFICIENTS

Film coefficients on the Votator side and jacket side were calculated. It is well known that the heat transfer is mainly dependent on the rate at which the heat can be transferred across the stagnant films which lie close to the metal. Although only a few thousandths of an inch thick, these films act as insulators and retard the flow of heat.

The heat Q which is transferred per unit time from the Votator to the jacket must flow through each resistance (1) Votator water

film, (2) metal, and (3) jacket-water film. The heat equation is then

$$Q = A_v A_m (t_v - t_m) \quad (2A)$$

$$Q = A_m A_s (t_m - t_s) \quad (2B)$$

$$Q = A_s A_j (t_s - t_j) \quad (2C)$$

Proportionality constants A_v , A_m , and A_s apply to Votator water, metal, and jacket-water film, respectively; t_v , t_m , t_s , and t_j , apply to temperature of votated water, metal surface on Votator side, jacket-water, and metal surface on jacket side, respectively. The area stays constant. This is an arbitrary assumption because U is based on the Votator side; this means only that the A values, even though applying to different films, are based on the area of the inside scraped surface. To convert to the outside area—e.g., $Q = A_v A_m (t_m - t_s) = A_s A_j (t_s - t_j)$. Then

$$A_v A_m = A_s A_j \quad (2D)$$

From Equation 2,

$$Q = \frac{1}{A_v} + \frac{1}{A_m} + \frac{1}{A_s} \quad (4) \quad U = \frac{1}{A_v} + \frac{1}{A_m} + \frac{1}{A_j} \quad (5)$$

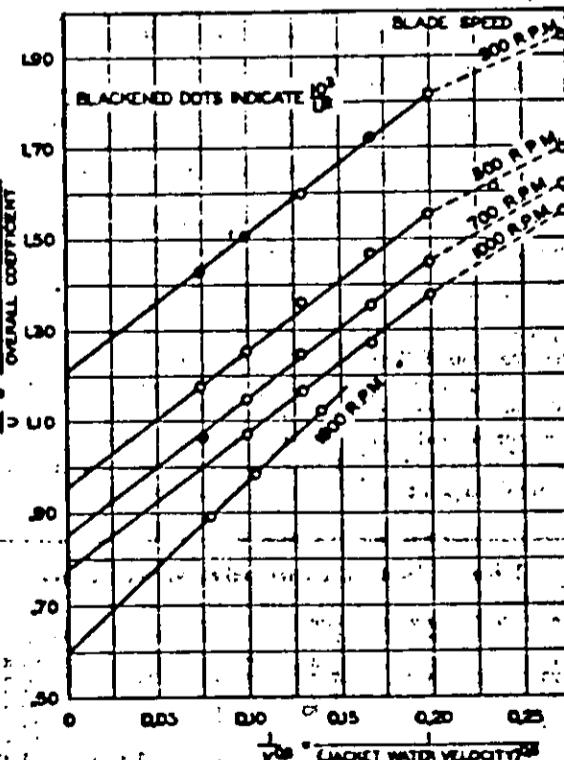


Figure 5. Reciprocal Plot for Film Coefficient Calculation

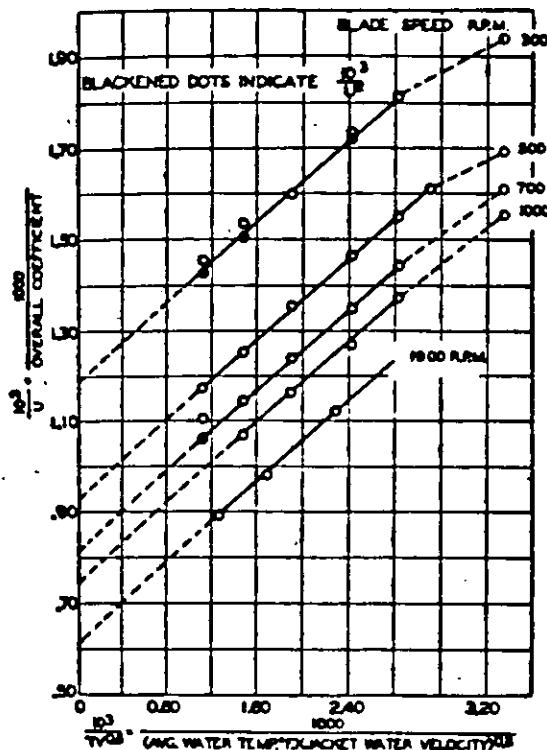


Figure 6. Reciprocal Plot Including Temperature for Film Coefficient Calculations

The coefficient for metal equals the thermal conductivity divided by the thickness of metal,

$$A_m = k/t \quad (6)$$

and may be replaced in Equation 5.

JACKET-WATER COEFFICIENT A_j . Empirically it has been shown (1, 2, 3) that in flow of water through pipes the film coefficient varies as the 0.8 power of velocity. Inside the Votator there are conditions which differ considerably from flow through a pipe, but in the jacket these conditions are fairly representative. This method was tried to calculate the jacket water film coefficients.

Maintaining a constant mutator speed should keep the Votator film coefficient, A_j , approximately constant, and $1/A_j$ should vary with $1/U$ (Equation 5); since it was shown that A_j varies with Vw , a plot of $1/U$ against $1/Vw^2$ should give a straight line for any given mutator speed. Substituting in Equation 5,

$$\frac{1}{U} = \frac{m}{Vw^2} + \left(\frac{1}{A_m} + \frac{1}{A_j} \right) \quad (7)$$

A plot of $1/U$ against $1/Vw^2$ is given in Figure 5. A straight line does result so that the assumption of constant A_j is justified. With the exception of 1900 r.p.m. the lines are parallel. The slope is 0.00303 and the jacket-water film coefficient A_j is, therefore, easily calculated.

There is about 5° F. difference in the jacket water used at 1900 r.p.m. and that for the data at 300-1000 r.p.m. This accounts in part for a difference in slope in these two sets of data. If no difference in slope had been obtained, it would have been concluded that temperature did not affect the jacket-water film coefficient, which is known to be false. The slope in this case is 0.00377. The intercepts of these lines from Figure 5 are:

R.P.M.	Intercept	R.P.M.	Intercept
300	1.208×10^{-3}	500	0.778×10^{-3}
700	0.355×10^{-3}	1000	0.307×10^{-3}
1900	0.255×10^{-3}		

The jacket-water film coefficient is calculated from

$$A_j = m/Vw^2 \quad (8)$$

Applying this method of calculation, the following results are obtained:

300-1000 R.P.M.				1900 R.P.M.			
Velocity ft./sec.	A _m / temp. °F.	A _j	A _j / temp. °F.	Velocity ft./sec.	A _m / temp. °F.	A _j	A _j / temp. °F.
25.9	65.8	4110	6450	23.9	60.3	3250	3250
18.1	66.6	3100	3260	17.1	61.6	2570	2570
13.9	67.8	2350	2560	11.6	62.9	1830	1830
9.8	69.2	1820	1972				
7.5	70.4	1480	1660				

Below a velocity of 7.5 feet per second the curve is no longer straight, and this method no longer applies. The black dots of Figure 5 do fall on the straight line so that the previous use of these values was justified. Since Equation 8 holds only in the turbulent region, it must be concluded that complete turbulence starts around 7.5 feet per second in the jacket of this Votator. From this work there appears to be a transition range in turbulence since Reynolds numbers were high (16,000) even when the jacket water velocity was 4.7 feet per second.

Since the temperature of the jacket water was different for the values at 1900 r.p.m. as compared to those at 300-1000, $1/U$ was plotted against $1/Vw^2$ in order to find out if the values at 1900 r.p.m. would fall into line (Figure 6). The 1900 r.p.m. points fall on a straight line parallel to the others. Therefore we are justified in correcting the value of A_j for temperature differences. The slope is 0.221. The film coefficients thus calculated were used in all later work:

300-1000 R.P.M.			1900 R.P.M.		
Velocity of ft. ft./sec.	A _m	A _j	Velocity of ft. ft./sec.	A _m	A _j
25.9	2760	4075	23.9	3250	
18.1	2840	3080	17.1	2570	
13.9	3190	2370	11.6	1830	
9.8	1780	1872			
7.5	1480	1660			

Comparison of this table with the one above shows that A_j (300-1000 r.p.m.) decreased about 10% when the temperature correction was applied.

VOTATED WATER COEFFICIENT A_v . The film coefficient on the scraped surface may be calculated by substituting in Equation 5 or 7. Equation 7 gives the following results:

Mutator Speed, R.P.M.	Peripheral Speed, Ft./Sec.	A_v for Scrapped Surface	Temp. of μ_w , °C.
	Fig. 5	Fig. 6	
300	8.92	1080	1110
500	8.54	1490	1550
700	8.16	1760	1870
1000	8.11	2030	2160
1900	94.8	3200	3030

Approx. same
Approx. 5° lower

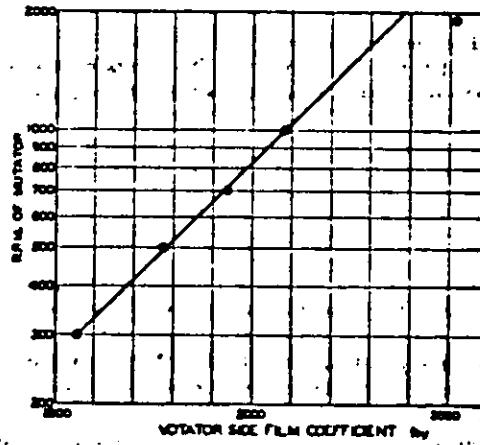


Figure 7. Relation between Blade Speed and Film Coefficient

June, 1944

Agitation and Mixing

STAINLESS STEEL TUBES OVER 1/2 IN. DIA.

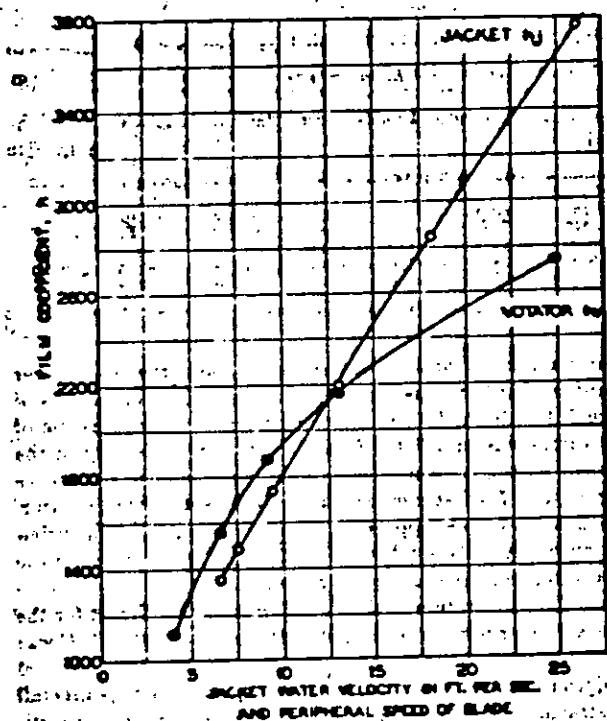


Figure 8. Effect of Velocity on Film Coefficients of Jacket and Scraped Side

The results from Figure 6 are plotted in Figure 7. The latter shows that the relation between film coefficient and rotator speed may be expressed by a straight line on semilog paper when jacket conditions are approximately the same. The equation is:

$$\log (r.p.m.) = m_1 h + \log (\text{intercept}) \quad (9)$$

$$= \frac{(0.475) h}{1000} + \log 87.5$$

The 1900 r.p.m. point falls to the right of the line; this may be due to the fact that the mean temperature of the rotated water (187° F.) was lower than that for the 300–1000 r.p.m. points (145° F.). Apparently, when thin liquids are used, a lower mean temperature inside the Votator leads to a higher film coefficient. This is unexpected, since, in general, with other heat transfer equipment the film coefficient increases with higher temperatures. The reason may be that the scraping force of the blade is more effective as the viscosity increases. The most effective equation for A_f is to express it as a function of the properties of the material processed; future work will attempt to set up such an equation.

COMPARISON OF A_f AND A_s . It is interesting to see how A_f and A_s vary for a given linear velocity. In the case of A_f , the velocity is assumed to be that of the tip of the blade. Figure 8 is a plot of A_f and A_s against velocity. The points on the A_f curve above 1000 r.p.m. are obtained from the extrapolated curve of Figure 7.

Figure 9 was constructed from Figure 8 by reading A_f and A_s at the same altitudes. The equation of this line is:

$$\log A_s = m_2 h + \log b \quad (10)$$

$$m_2 = -0.386/1000; b = 324$$

Thus when A_f is known, A_s can be calculated from Equation 10 and vice versa. The effect of changes in operating conditions on this curve is not known. Equation 10 at first appears to have no immediate application, since to determine A_s would, in general, give the experimental means for obtaining A_f . However, the following section shows that the Dittus-Boelter equation can be used to obtain A_s and thus obtain A_f on the basis that Equation 10 holds for other operating conditions.

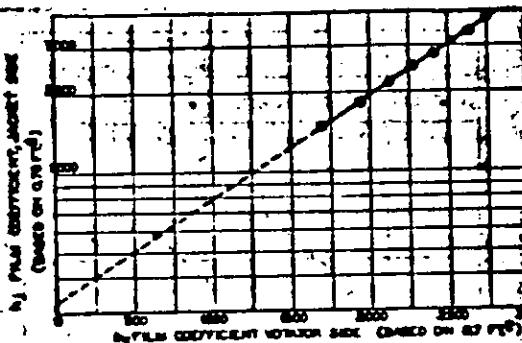


Figure 9. Relation of Film Coefficients during Votating

A_f BY DITTUS-BOELTER EQUATION. Dittus and Boelter (7) were able to show that, for a wide variety of materials (e.g., air and water) flowing in turbulent motion, the film coefficient of heat transfer could be represented by the empirical equation,

$$A_f D/k = 0.0225(Re)^{0.8}(Pr)^{0.4} \quad (11)$$

where D is the diameter of the pipe; in the case of the Votator jacket it is D_s , the equivalent diameter of the rectangular helix.

The following table summarises the different water velocities used in the Votator jacket and compares them to the values of A_f obtained from Figures 5 and 6:

Velocity, ft/sec.	m_2	U (Fig. 5)	U (Fig. 6)	A_f from equation	D_s & R
22.9	-0.386	3110	3070	3240	2110
18.1	-0.386	2190	2140	3110	2110
15.0	-0.386	2250	2190	3430	2080
9.8	-0.386	1820	1770	3110	1770
7.5	-0.386	1530	1480	3240	1480

The results are in good agreement. A fairly accurate estimation is therefore available of A_f and of A_s from Equation 10; or if the over-all coefficient has been determined, A_f can be more accurately obtained from Equation 5. Also the calculated A_f falls closer to A_f obtained from Figure 5 than from Figure 6. This is, however, no criterion of selection since A_f is not known with sufficient accuracy, and A_s could easily vary by 10%.

DIFFERENT VOTATING CONDITIONS. The data graphed in Figure 4 for two throughput rates (340 and 580 pounds per hour) at 1900 r.p.m. can be treated similarly by the methods outlined.

These data are plotted in Figure 10 for $1/U$ against $1/T^{1/2}$. Here, as previously, the lines are not parallel when $1/U$ is plotted against $1/T^{1/2}$ since the jacket water temperatures were different. The method of dividing by temperature again shows its merit since the slope for the two rates, even though of different jacket-water temperatures, became the same. From Figure 10, the corrected film coefficients are as follows:

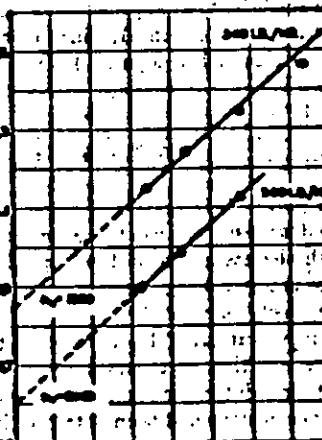


Figure 10. Reciprocal Relation Comparison, including Temperature, Coefficients, and Different Votating Conditions for Film Coefficient Calculation

340 Lb./Hr., $A_1 = 1800$		
Av. j_w	V. of j_w , ft./sec.	A_1 , Fig. 10
55	34.25	3410
60	37.0	2620
61.5	31.75	1900
63.6	31.13	1840

580 Lb./Hr., $A_1 = 3140$		
Av. j_w	V. of j_w , ft./sec.	A_1 , Fig. 10
60.3	33.9	2580
61.6	17.08	2620
63.6	11.6	1900

Even though the average temperature inside the Votator is considerably different, this alone does not seem to explain the marked change in A_1 with change in rate. Further work is necessary to clarify this point.

SUMMARY

1. A good average over-all coefficient is about 800 B.t.u./hour (square foot) ($^{\circ}$ F.). The coefficient varies as follows:

Motor Speed, R.P.M.	Velocity of j_w , ft./sec.	Overall Coefficient, U
300	5	800
1800	24	1120

2. A minimum jacket-water velocity of 7-10 feet per second and a minimum motor speed of 600 r.p.m. (7.8 feet per second) should be used for efficient operations on waterlike materials. Values greater than these are beneficial and should be used if other factors such as power load, jacket-water pressure drop, blade and tube wear, do not make the operation uneconomical.

3. The film coefficient on the jacket side varies about as follows:

Velocity of j_w , ft./sec.	A_1 , B.T.U./(Hr.) (sq. ft.) ($^{\circ}$ F.)
7.5	1800
24	4100

4. The film coefficient in the rotated water side varied about as follows:

Motor Speed, R.P.M.	Peripheral Speed, ft./sec.	A_2 , B.T.U./ (Hr.) (sq. ft.) ($^{\circ}$ F.)
300	3.9	1100
1800	13.1	2200

5. The Dittus-Boelter equation can be used to calculate the film coefficient on the Votator jacket, even though the path is helical. The results check experimental values within 10%.

ACKNOWLEDGMENT

The author wishes to thank Bruce E. Adams for his help with the calculations and figures presented here.

NOMENCLATURE

- A = cooling surface area, sq. ft.
- D = equivalent diameter of jacket based on rectangular section
- G = mass velocity, lb./sq. ft./sec.
- A_1 = film coefficient of heat transfer, B.t.u./(hr.)(sq.-ft.) ($^{\circ}$ F.)
- A_{jw} = jacket-water film coefficient based on inside area on heat transfer wall
- A_{ow} = jacket-water film coefficient based on outside area of heat transfer wall
- A_m = metal wall expressed as film coefficient
- j_w = jacket water
- $LMTD$ = log mean temperature difference, $^{\circ}$ F.
- l = thickness of metal
- Motor = shaft with scraper blades
- ΔP = pressure drop through water jacket, lb./sq. in.
- P_r = Prandtl number = $c_p/\mu/k$
- Q^* = heat transferred, based on heat removed from rotated water, B.t.u./hr.
- R_e = Reynolds number = DG/μ
- T = temperature, $^{\circ}$ F.
- U^* = over-all coefficient based on Q^* , B.t.u./hr.(sq.-ft.) ($^{\circ}$ F.)
- V = velocity, ft./sec.
- * See footnote Table I.

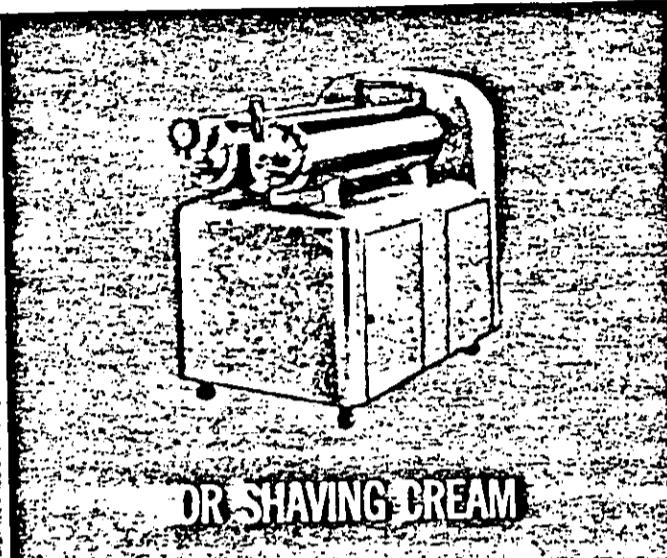
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- (1) Dittus, F. W., Boelter, L. M. K., *Trans. Am. Inst. Pub. Engrs.*, 2, 443 (1930).
- (2) McAdams, W. H., Sherwood, T. K., and Turner, R. L., *Trans. Am. Soc. Mech. Engrs.*, 48, 1233 (1926).
- (3) Wilson, L. E., *Ibid.*, 37, 47 (1915).

Patented in U. S. A.



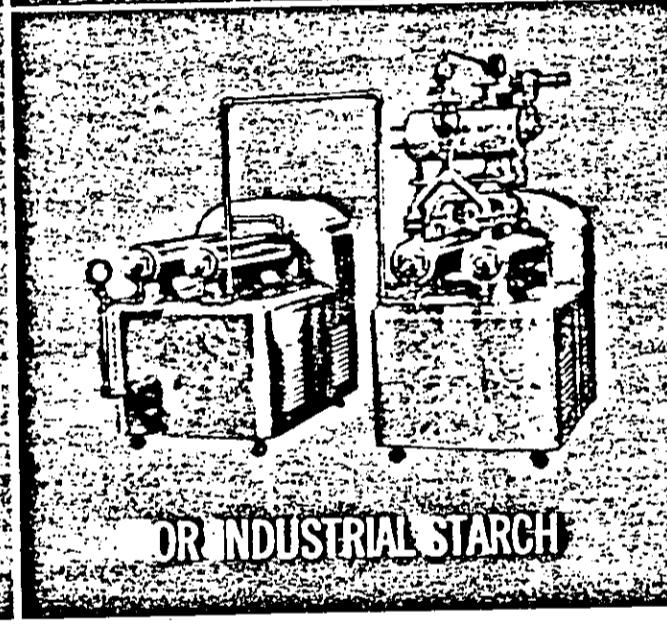
LUBRICATING GREASE



OR SHAVING CREAM



OR PARAFFIN WAX



OR INDUSTRIAL STARCH

OR

What viscous material can you
process more profitably?

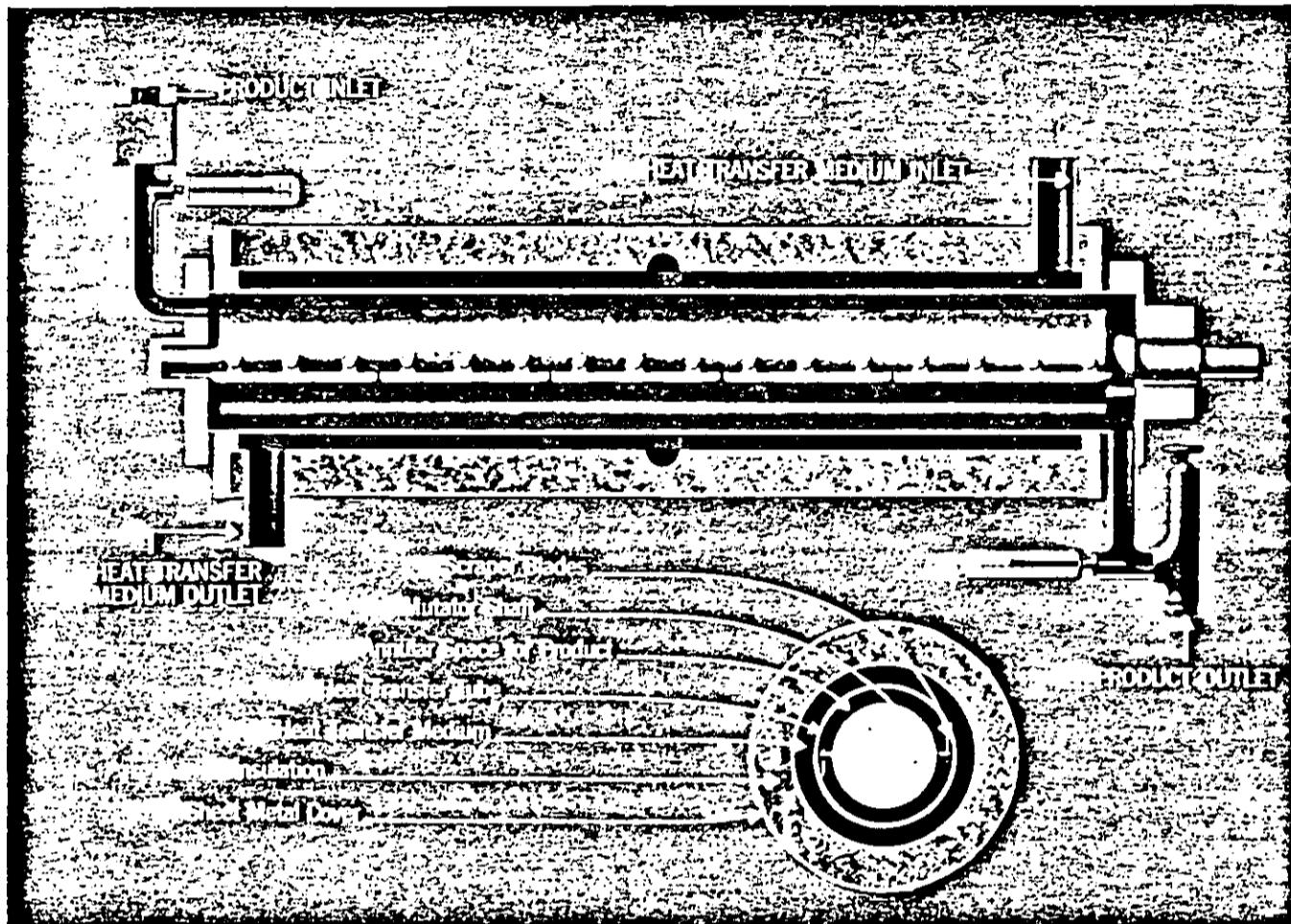
ALMOST invariably the processing of viscous materials involves heating or cooling. Votator equipment provides a continuous, closed system embodying the cleanest, safest, most efficient heat transfer operation for this purpose. Does a dependable, more uniform job in generally less than half the floor space required by batch methods. Makes possible corresponding savings in labor, heat or refrigeration, and overall operating expense for a great cross-section of industry.

The above were picked at random from more than a dozen tried and proved Votator applications. There is also a long list of potential Votator applications which may include your products—the processing of viscous materials covers such a wide range of industrial territory.

If you process anything in viscous form which requires heating, cooling or both heating and cooling, chances are Votator equipment can cut your costs, increase your profits.

Votator
A GIRDLER PRODUCT

6/6/5



VOTATOR Systems have this heat transfer mechanism

VOTATOR equipment is setting new records for efficiency in the processing of liquid and viscous products which require heating, cooling or both heating and cooling.

This exclusive, patented heat transfer mechanism is one of the reasons why.

It is the most effective application known of the basic theory that a clean heat transfer surface together with a high ratio of heat transfer surface to volume of

material being treated, does the best heat transfer job.

The material is forced into a narrow, annular passage, there contacts the heat transfer surface as a thin film. Revolving scraper blades constantly expose a clean surface to the material.

The material is heated or cooled, as the case may be, almost instantly. This takes place under pressure, non-stop, and a remarkable volume is handled in relation to the size of the equipment.

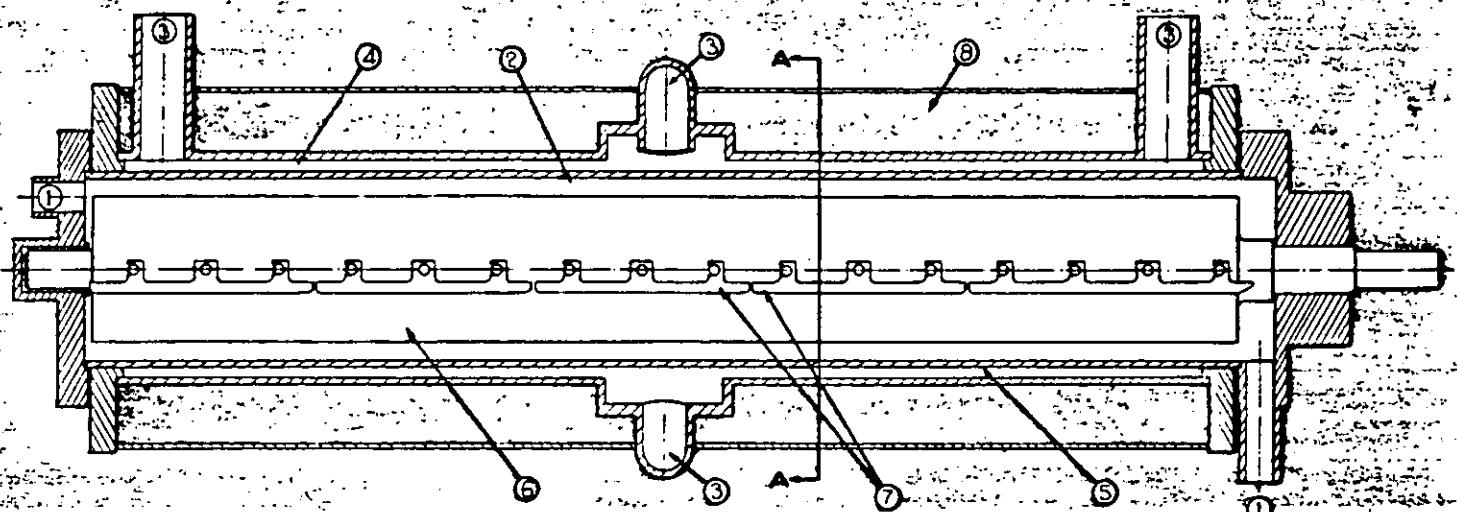


VOTATOR—U. S. Pat. Off.

THE GIRDLER CORPORATION, VOTATOR DIVISION, LOUISVILLE 1, KENTUCKY

DISTRICT OFFICES: 150 Broadway, New York City 7 • 2612 Russ Bldg., San Francisco 4 • 617 Johnston Bldg., Charlotte 2, N. C.

DIAGRAMS OF VOTATOR MECHANISM

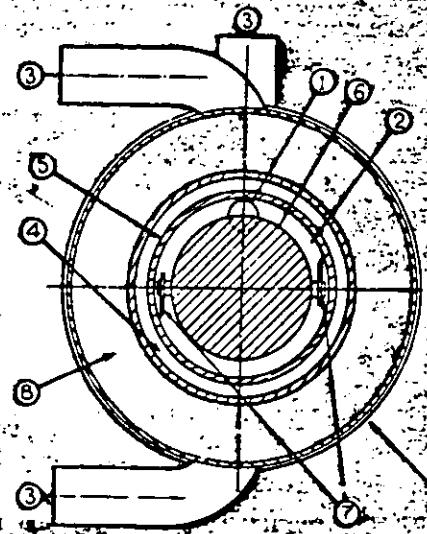


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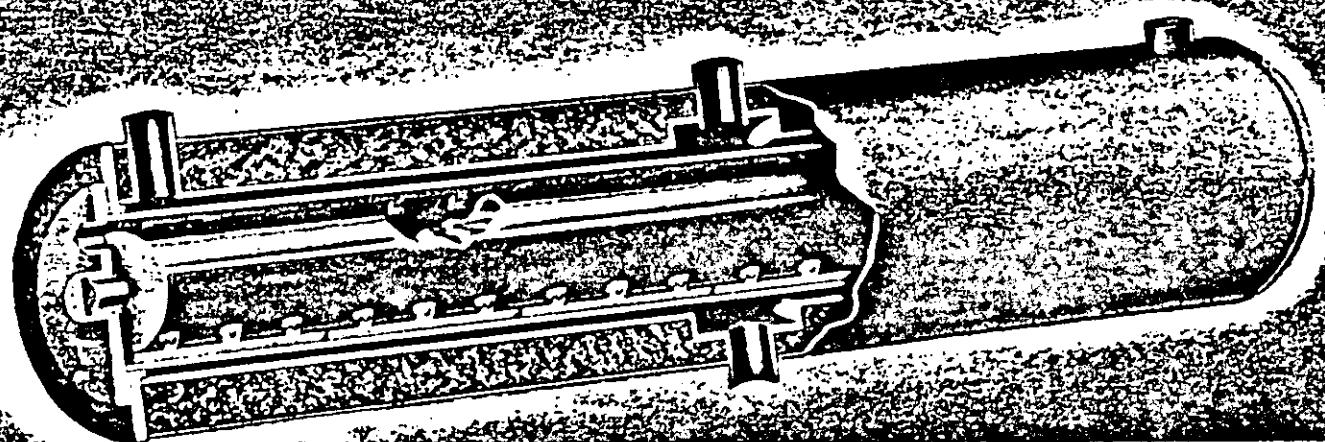
- 1. Product Connections.
- 2. Annular space thru which product passes.
- 3. Heat Transfer Medium Connections.
- 4. Annular space thru which heat transfer medium passes.
- 5. Heat Transfer Tube.
- 6. Motor Shaft.
- 7. Scraper Blades.
- 8. Insulation.

How the Votator Unit Operates

The material being processed is pumped in connection (1) thru annular space (2) and out connection (1) at opposite end, depending upon direction of flow desired. The heating or cooling medium enters at connection (3), passes thru annular space (4) and out connection (3), the actual piping arrangement to be determined by the type of heating or cooling medium used and the direction of flow required. The motor shaft (6) carrying scraper blades (7) is motor driven, causing blades to scrape film from surface of heat transfer tube (5) several hundred times per minute.



SECTION A-A



1-15-47

(7) Hydroxylation of acetylenic Hydrocarbons

C.A. 39, 741 (1945)

U.S. Patent 2,347,358 April 25, 1944

Nicholas A. Nicas (to Research Corp.)

Saturated org. compds. containing the acetylenic linkage $-C\equiv C-$ such as C_2H_2 , monosubstituted acetylenes of the type $R-C\equiv C-H$ and disubstituted acetylenes of type $R-C\equiv C-R'$ where R and R' are uni- valent organic radicals, are treated with H_2O_2 in an anhyd. inert organic solvent in the presence of a small amount of O_2O_4 , RuO_4 , V_2O_5 , MnO_2 , or CrO_3 in the absence of an organic base. The resulting products are hydroxy aldehydes and (or) hydroxy acids.

Note - C.A. 31 to C.A. 39
(1937) to (1945)

covered as to oxidation (by air or otherwise) of $-C\equiv C-$ with a nil result.

11-20-46

Synthesis and degradation of a cyclic polyene
C.A. 40, 3394^a (1946).

A. Babayan - Bull. Armenian Branch Acad. Sci.
U.S.S.R. 1941 no 5/6 (10/11), 121-
45 (in Russian)

B) dehydrate d 2,5-Dimethyl-2,5-Dihydroxy-
hexane-3 with $\text{Hg} \leftarrow \text{SO}_4$ to yield (80%)



b.p. 123-124°C

G.r. 0.7863

It was accomplished by slowly distill-
ing the ketone from the sulfonic acid
under vacuum.

A. BROTHMAN & ASSOCIATES

No. 1 of
Date: 11-2-47

By: H.A.

JOB: Mettler

SUBJECT: $\text{Ca}(\text{OCl})_2$ Process

Step	Time	Rate
1. Estimate chlorine dilution required	20-40 sec	16.6
2. $\text{Ca(OH)}_2 + 2\text{NaCl} \rightarrow \text{Ca}(\text{OCl})_2 + 2\text{NaOH}$	10-12 sec	0.6
3. Filter	1-2 sec	1.66
4. Conduct final filtration as independent steps	1-2 sec	1.66
5. Dryer	1-4 sec	0.25
6. Anticipated total rate		1.66
7. Recovery can be increased with a dilutional line dilution, if a cut back is done in chlorine to sodium chloride ratio (from 1:1)		1.66

Step	Time	Rate
1. Recovery dilution	1. sec	1.66
2. Reactant	0.25 sec	0.25
3. Hydrochloric acid	0.25 sec	0.25
4. Rinse	0.25 sec	0.25
5. Rinse dilution	0.25 sec	0.25
6. Filter	0.25 sec	0.25
7. Drying	0.25 sec	0.25

(1)

11-18-46

Action of H_2O_2 on unsaturated Hc

Benzene 33, p. 2015 - 18 (1900)

C. F. Cope, C. J. Devan and Th. Neiburg
(co-workers with Fenton)

Action on Cu-Hc

1. add 0.125 gms. $FeSO_4 \cdot 7H_2O$ per 50 cc of diluted

(3%) H_2O_2 .

2. To this add the Cu-Hc (about 0.5 gm.) till the reaction is complete.
Keep the temp. at $50^\circ - 70^\circ C.$

3. Data - per 50 cc H_2O_2

: : reaction products

Run No.	H_2O_2 $\frac{g}{70}$	$H_3C-COOH$	EtOH	$H_3C-C\equiv N$
1	0.50	0.24	0.0009	0.0025
2	1.57	0.60	0.0014	0.0011
3	2.81	1.10	0.0015	0.0045
4	4.58	1.26	0.0019	0.0093
5	6.59	1.71	0.0016	0.0117
6	8.72	2.01	0.0010	0.0109
7	10.54	2.28	0.0004	0.0123

Note - Fenton, J. Am. Chem. Soc. 25, 1-11 (1899),
uses for iodine titrat. { 6.24 g. glycol
dissolved in 70 cc H₂O

11-18-46

- (②)
4. cool to room temp in ice and then let stand for 1/2 hrs.
 5. separate reaction product by forming
of a grom:

(4)

11-18-46

Oxidation of -C=C-COOH acid

org. Chemists 24, p. 38-40.

R. Reich, R.B. Mittell, & A.V. M. Hatch

oxidize complex aromatic end- containing
-C=C- side chain to the corresponding
acid.

Data

1. Diss. 0.1 mole of end in 200 cc AcOH

2. add a soln. of { 37 gms. CuO
} dimethyl
ethanol { 50 cc H₂O
per
200 cc. of AcOH

3. keep temp at +10°C

4. addition should take 10 min.

5. keep temp at 50°C for addnl. 20 min.

6. cool soln. (2°?)

7. destroy excess copper acid by adding

50 cc. of MeOH - keep 2° below 50°C.

8. conc. reaction mass by distillation

under reduced pressure

9. distil rapidly at first; then very slow & below

30°C; at 10 mm. the conc. requires about

2 hrs.

(5) 11-19-46

oxalic acid from acetylene

J.A.C.S. 45, 795-9 (1923)

R.L. Kearns; L. Shier & J.A. Nicol and

Data

1. three flasks are connected in series to a manometer
2. in each flask is placed a mixture of
$$\begin{cases} 900 \text{ cc. conc. HNO}_3 \text{ (sp.gr. 1.42)} \\ 500 \text{ cc. H}_2\text{O} \\ 25 \text{ gms. Hg(NI)}_2 \end{cases}$$
3. acetylene and air (at 70 mm) are passed into the first flask and then the other two flasks. The first flask is agitated.
4. when the reaction in the first flask has moderated, the first and second flasks are transposed and the process repeated till all three flasks had been exchanged.
5. the three mixtures are then combined and C₂H₂ passed in till all evidence of reaction has ceased.
6. the oxalic acid separates in crystalline form. (It is washed with distilled H₂O.) The yield is approx. 1000 gms. (dried)

11-18-46

Formation of cyclohexane γ -glycols

C.A. 31, 5793^b [T. Sato. Ann. (U.S.S.R.)]

Tetrahydrobutteric diol is oxidized to

2,2,5,5-tetrahydro-3,4-dioxotetahydrofuran

5 g. tetrahydro and dis in 25 cc 17% H_2O_2 (dilute)

add 2.56 g. CuO, dilute in 25 cc of 95% H_2O_4
dropwise + stirring.

Ext. furan and with petroleum ether.
yield 51%.

11-19-69

Reaction between O_2 and acetylene in the presence of nitrogen oxides

J. A. C. S. 53, 2962-7 (1931)

S. Lihmer

C₂H₂ is oxidized by O_2 thus:

Nitric acid vapor is introduced into a gas mixture of 1:1 C₂H₂ and O_2 by first passing the O_2 thru a small bottle containing 90% HNO₃ and only 0.046% nitrogen peroxide.

Data (partial) { 190 cc of 1:1 C₂H₂- O_2 used
contact time = 3 min.

Temp., °C	HNO ₃ in mixt., %	Reaction Products				
		C_2O , %	CO, %	H ₂ %	Alcohol, %	Acetone, %
210	1.7	0.3	5.2	0.1	0.0132	
230	1.7	1.1	4.2	0.2	0.0150	
210	4.1	3.4	19.1	0.3	0.0362	
230	4.1	6.2	20.1	0.3	0.0418	

Principal reaction product is trimethyl alcohol, corresponding to 50-60% of the acetylene oxidized.

4-20-47

Ann. de la Société Chimique 25, 346-369 (1911)
methyl bromine

Formation & Recovery of acetals

1. Reacted material in stated tubes under the
following conditions: time 3-6 hrs.
 $\text{H}_2\text{O}_2 \approx$
- dim.

1 H-0	0.79	13 H-0	0.245
2 H-0	0.69	32 H-0	0.195
4 H-0	0.57	64 H-0	0.061
7 H-0	0.42	107 H-0	0.000

* dim = fraction of
methyl bromine

2. Found hydrolysis takes place best with H_2O_2

$\leftarrow \text{H}_2\text{O}_2, \leftarrow \text{AcOH}$.

3. Other results - cold

methyl + 16 H-0 @ r.t. \rightarrow $< 1\text{ part}/1000$
methyl + methyl acetate

methyl + 16 H-0 @ $14-16^\circ\text{C}$ $M_2 \frac{M+2}{7-2}$

H_2O_2	16 H-0	H_2O_2	H_2O_2
Time	11	7	7
5	0.77	17	0.71
28	0.45	47	0.60
216	0.30	163	0.38
		69	0.75
		191	0.55

(2)

4-20-47

Methylal + 128 H₂O Q 14-16°C

		H ₂ O		H ₂	
T	M	T	M	T	M
21	0.54	16	0.97	3	0.96
70	0.24			21	0.77
120	0.096	120	0.79	289	0.14

16 H₂O 120 H₂ 2 = 0.503

120 H₂O 120 H₂ 2 = 0.03

T	M	T	M
18	0.72	21	0.65
69	0.26	46	0.36
113	0.09	70	0.21

4-20-47

Graph. Num. 36, 4-20-1947

Decomposition of methylal in gas phase
among other coms.

E-T. testing

methylal decomposed in the gas phase at 410°C
in a quartz vessel, doubling its pressure in
about 51 minutes & then changing slowly
without reaching equilibrium after 7 hrs.

acet al \rightarrow pressure nearly 3 times original
at 370°C indicating that the acet al
molecule breaks up into two molecules.

Benzene 70, 1713 - 1719 (1957)

Hydrolysis of acetals

J. Gobeyn & A. Fleischmann

$$k_{\text{obs}} = \frac{1}{(t_2 - t_1) 0.4562} \log \frac{a - v_0}{a - v_1}$$

$$k' = k_s \text{ (hydrolysis constant)}$$

corr of
and
catalyst

30°C	t ₂ - t ₁	a ₀	a ₁	k
$k_s = 5.3 \times 10^{-3}$	40	1.23	25.4	5.2×10^{-3}
$k_s = 3.91 \times 10^{-3}$	245	4.06	74.8	3.45×10^{-3}
	43.6	4.97	91.0	3.40×10^{-3}
	71.0	5.16	100.0	—

2.

°C K_s

70 0.56 $\times 10^{-3}$

44.17 0.74 *

20 1.22 *

25 1.83 *

30 3.01 *

35 8.86 *

private 67, 424 - 9-9 (1954)

6-6-47

velocity of actual hydrolysis

M. H. Palomaa & Aine Salonen

$$C_A = \text{actual normality} \quad k = \frac{1}{t_2 - t_1} \ln \frac{(V_i - V_{\infty})}{(V_r - V_{\infty})}$$

$$C_{AH} = \text{true normality} \quad \frac{\text{velocity}}{\text{constant}} \text{ time} = 1 \text{ minute}$$

for methanol

$$C_A = 0.3065$$

$$C_{AH} = 0.557$$

$$k_{2,5} = 0.00187$$

$$k_{3,5} = 0.00860$$

$$\frac{k_{2,5}}{k_{3,5}} = 4.56$$

also,

$$C_A = 0.3$$

$$C_{AH} = 0.15$$

$$k_{2,5} = 0.00153$$

201
202
203
204

SAC, Philadelphia

7/10/50

SA T. SCOTT MILLER, JR.

HARRY GOLD, was.
ESPIONAGE - R

EXHIBIT 65-4307-1B-13 (10) (Exhibit 21)

On 6/22/50, GOLD was shown the above material, at which time he stated that the letter on the stationery of the ACHESON COLLOIDS CORPORATION was from his friend, MORRELL E. DOUGHERTY.

PRESTO SALES, the name which appears on the envelope, made acetylene, and the BROTHMAN firm purchased same from PRESTO.

The remainder of the material is concerned with work at the BROTHMAN firm.

TSM:HKP
65-4307

1. Vapor phase esterification
2. Hydration of chloroformic acid
3. Hydrating action of H_2SO_4 at various temperatures
4. Decomposition temperature of chloroformic acid
5. Dent. agr. work on dehydratation of α -OH-butyric acid

Aug 37, 1946
MEMORANDUM

4-5 2, 416, 5C,

cure E. Ritter (to U.S.D.A.)

~~anhydride~~ ~~methacrylic acid~~
~~methacrylic acid~~ ~~methacrylic acid~~
mixture with acrylic acidscure He 1.p. 58-61% → quaternary
with MeOH.

2. To about one liter with 1.p. 50-51%

~~below~~ ~~top~~ ~~of~~ ~~quaternary~~ ~~below~~
~~above~~ ~~top~~ ~~of~~ ~~quaternary~~ ~~below~~
~~above~~ ~~top~~ ~~of~~ ~~quaternary~~ ~~below~~
methacrylic acid

4.1

92.4 EtOH

81.6g. methacrylic

11.4 H₂O101.6 H₂1. reflux → 48% ~~solid~~ ~~solid~~

2. Distill 48-50% → MeOH + 1/2

3. add inhibitor, reflux & take off

4. 2 (100)

1. wash - reundate acetone + PbO + C

2. add 10% H₂O to 3 of acetone distilled
well by with HeMeOH
EtOH46.48%
80.83%
56.51%66.50
70

ACHESON COLLOIDS CORPORATION
PORT HURON, MICHIGAN

MEMORANDUM

To _____

SUBJECT _____

SUB-HEADING _____

REFERRING TO _____

LETTER OF _____

COPY TO _____

FROM _____

DATE _____

Harry -

Wish you luck - see you
over the week-end.

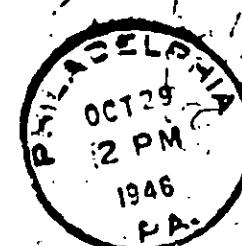
Doc

ACHESON COLLOIDS CORPORATION

LAND TITLE BLDG.
PHILADELPHIA 10, PENNSYLVANIA

SPECIAL
DELIVERY.

Prieto
Sales
10-10-60
9-2-60
9-2-60
9-2-60



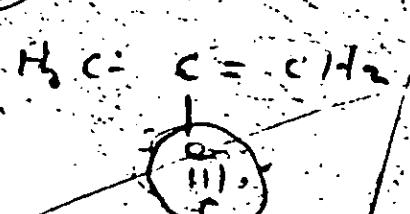
Mr. Harry Gold
c/o ABA Laboratories,
8503 - 57th. Ave.,
Elmhurst, L.I. New York.

6-6-50

44-13-C



H₂C=CH₂



104

48
142

~~H. C. C. C. H.~~

三

1

H. C.

1

三

1. Venturi-type off-still Head.

1. Lab. designed "Nurse Triple" capable of
delivering ~~a~~ a. i. p. g., oxygen stream

~~one~~ for $7\frac{1}{2} \times 11$ " with Diverter
valve Flange & equipped with a
dead providing for

- a - agitation
- b - a dosimeter tube
- c - a tube-off tube

U - F. Dolard

1. g mol CH_2O : 1 ab. min.

Take up in Cu kettle to w.s. tube \rightarrow 500 ml
water - 100 ml

Killed with Et iodide to stop the Et cutting
use a Σ flask over 500 ml min

dry on trays. (\rightarrow drying)

mill (2-2 mill)

Catalysts are added - anhydrite NH_4Cl

Granulated (coarse to smooth)
(1 mm)

3. avoid dusts - special

R.C.

1. set up your tools before starting

2. Et cell.

3. small mill

4. Granulator

solubility of p-dichlorobenzene

p-dichlorobenzene in C₆H₆

5°C

75 ml. C₆H₆

$$\begin{array}{r} 100.0 \\ - 32.7 \\ \hline 4 \mid 67.3 \text{ ml. p-dichlorobenzene} \\ \hline - 11.8 \end{array}$$

$$\begin{array}{r} 100.0 \\ - 26.8 \\ \hline 73.2 \text{ ml. p-dichlorobenzene} \end{array}$$

20°C

65-143-7
22

SAC, Philadelphia

7/10/50

SA T. SCOTT MILLER, JR.

HARRY GOLD, was.
ESPIONAGE - R

EXHIBIT 65-4307-1B-13 (11) (Exhibit 22)

On 6/25/50, GOLD identified the notebook pages comprising this exhibit as being his handwritten notes in connection with a chemistry course at the University of Pennsylvania, as well as a German course at the same institution.

It is noted that these notes are dated 1932.

TSM:HKP
65-4307

27/3/5 ✓

Localization of Industries

i) H. Soc & Refinery

large no. of small plants

(a) Petroleum Refinery

expensive labour is capital intensive. product of low bulk value i.e. refineries are near markets

b) Rubber

Rubber must be imported. British control market. Has high bulk weight. Transport costs are not a trifling factor.

Rubber is a laboratory product throughout. produced in small batches. Do not tend to ship this any great distance to consumer.

3) Salt Industry
where raw material exists

(a) Coal Gas & Chemicals
located where greatest ^{raw} material & greatest demand for them exists.

ii) Paper & Pulp. - produces own products & does not depend on other products.

iii) Rayon material

iv) Soap

3. enormous quantity of high grade water
4. required practically no production of pulp in Phila. originally used to bring in wood, but now bring in as paste in a drum or dry in sheets.
5. use grain stalks for feeding high grade paper

5. Clay Products - little bulk value, no carrying charges. In addition due to processes which require considerable fuel and skilled labor.
Glass industry - can always glass rods good sand

Fuel in U.S.C.
see page 23 of text book

7. cuttings

Capital ratio -

1. If for every \$ million of capital invested ratio is one \$ millions invested ratio is high
2. if capital ratio is high
3. more receivables and the cost of financing products
4. stock of finished products is large and obsolete
5. equipment obsolete
6. sufficient utilization of labor

next. Specific industries
be able to tell what economic
factors control said industry

labor ?
raw material ?
market ?

16.50
80

concludes 1st Chap

Chap II

- Geographical Analysis of Industrial Areas
has been by no. small plants, more economical to send goods distant
far & cheap for pumping to within 5 miles
- natural has only competition
~~petroleum~~ refining
- Stages Part
 - 1. rubber industry ~~the~~ largest still labor
 - 2. clay products
 - 3. Growth of Industry
 - 4. Localization of Industries
 - see next p. 19
 - 5. a market det. by density of population
 - 6. one must consider all variables
 - in location of industry, market is greatest factor.
rubber industry near automobile industry

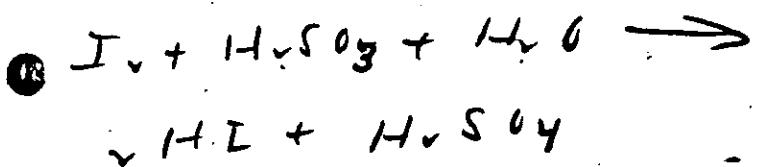
Wed. ~ 1/7/3 ✓
Dr. Lubens
text p. 551 - 593

Iodometric Processes

Iodometry

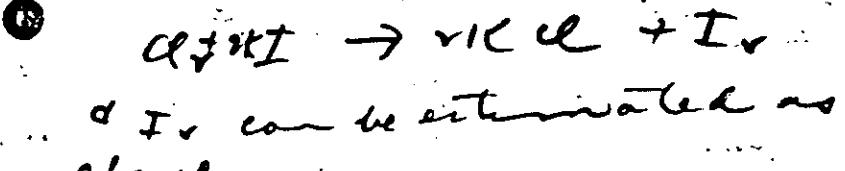
- Reaction of iodine with starch is very much influenced by temps. Color vanishes on heating & reappears on cooling. must be certain that solution is at room temp. or lower.

- I₂ may be produced by reaction or may be prepared as a std. reaction



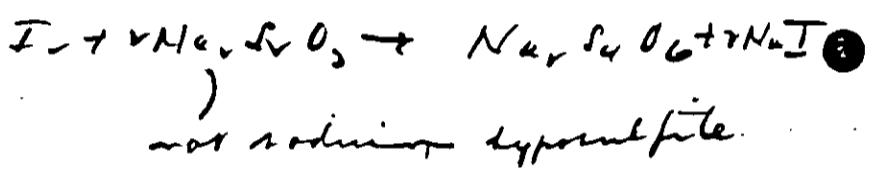
- Production of blue more easily recognized than vanishing of blue.

Free chlorine can be estimated by F method

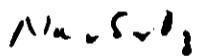


Bunzen found that the upper limit of strength of $H_2S_2O_8$ was 0.490. This could be used. Bunzen extended method to Br_2 , BrO_3^- , ClO_3^- , chromates, chlorates, iodates, vanadates, manganates, ferrates etc.

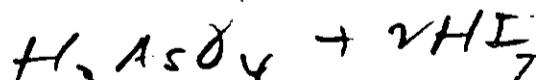
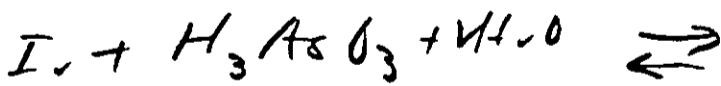
Inhibitor for $H_2S_2O_8$ proposed by Schwartz



replaced by Sni



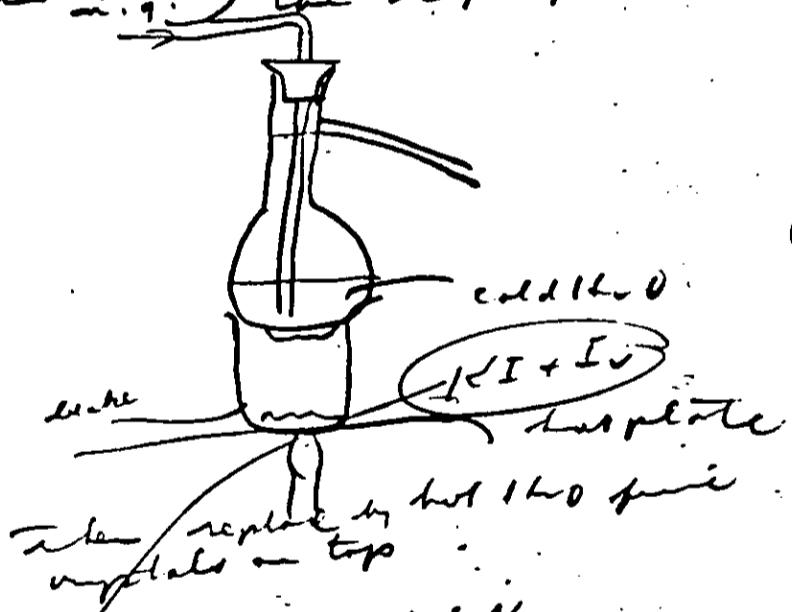
reaction is applicable to neutral or faintly acidic soln. but is not applicable to an alkaline soln. even a bicarbonate.



reversible because $[H^+]$ determines which way reaction goes

6/2/59

completing, if much difficulty
 in getting stops etc. just
 wait until certain that
 iodides are present and not
 mixed with other impurities.
 2 gms of standard liter.
 pres. of 1 to 2. not
 commercial I contains cl,
 n^o, staining etc. can be
 purified (elaborate methods
 in text!) can be prepared



to get rid of CN
 and sublimation is quite
 sufficient.

I₂ can be recd by diss. in KI + KI
 & using a weighing bottle



If was reaction to go from left
to right must have something
to react. H_2I

- If was reaction to go
from left to left must
have excess $[\text{H}^+]$ & lead
sol. to iodate I_3^-
 $\text{NaI} + \text{H}_2\text{O}_2 \rightarrow \text{NaIO}_3 + \text{H}_2\text{O}$
- $\text{I}_3^- + \text{NaI} \xrightarrow{\text{AsO}_4^{3-}} \text{NaIO}_3 + \text{NaI} + \text{H}_2\text{O}$

- Prepare fresh starch solution
as we need it, mix starch
in cold water & pour suspension
into boiling H_2O until we
have a clear fluid starch
solution.

- To keep starch sol. in small
bottles practically filled to
tops & tightly stoppered or
else use HgI_2 .

- may get violet or brownish
color as one approaches end
point. Can be avoided by
completing most of the
titration before the end
point is also starch is added
& then adding starch &

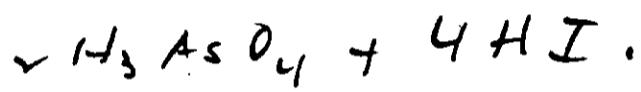
twice weight KI sol. + then
add I₂ crystals.

use a H/10 I sol.

- See text for more.

Can also use As₂O₃ as
std. can be obtained pure
must be sublimed or as a
little Se gives it a pronounced
yellow color. \rightarrow Se red color.

- $As_2O_3 + r. I. + 5 H_2O \rightarrow$



- weigh out As_2O_3 & dissolve
 \sim in H_2O sol.

- Det end point on blue
color with starch indicator,

know KI is sol. of I. about

- twice weight of KI as we
need I₂ in sol.

Wed. Feb. 4 1964

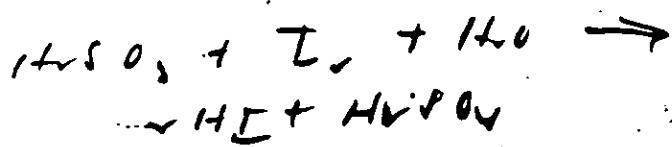
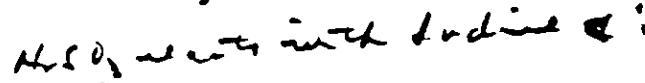
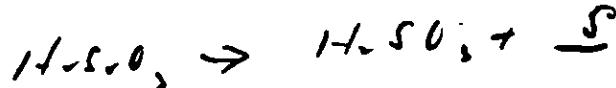
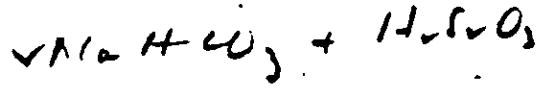
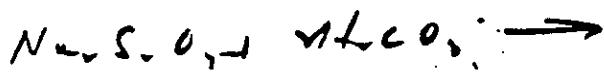
Dr. tubers.

Prep of $\text{Na}_2\text{S}_2\text{O}_3$ sol.

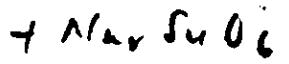
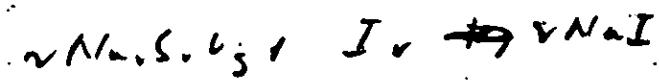
① Thoroughly cleaned

② Pre-weathered

(i) $\text{Na}_2\text{S}_2\text{O}_3$ sol metastable
as CO_2 dissolved in H_2O reacts
with $\text{Na}_2\text{S}_2\text{O}_3$:



the role of $\text{Na}_2\text{S}_2\text{O}_3$ now appears
to be stronger than before and



... sol as strong as the originally
made for $\text{H}_2\text{S}_2\text{O}_3$ reacts with
I₂

C or may be removed by
burning & will still battery a
if kept stoppered ad. will
not change.

Light has no appreciable effect.

I, solutions also are not suitable
must have convenient ~~method~~
for std. of I, sol.

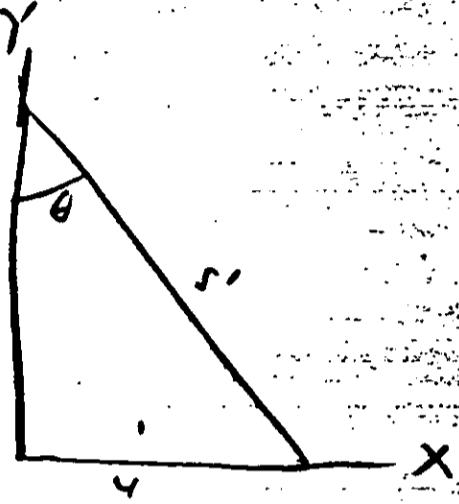
as I, sol is best made by
direct weighing out as described
in last lecture & should be
used only for standardization
& not for analytic end purpose

Pure Cu wire is best
test. method for det. of
 Na_2WO_4

overight carefully.
sample of pure Cu wire + diss.
 $\text{HNO}_3 \Rightarrow \text{Cu}(\text{NO}_3)_2$

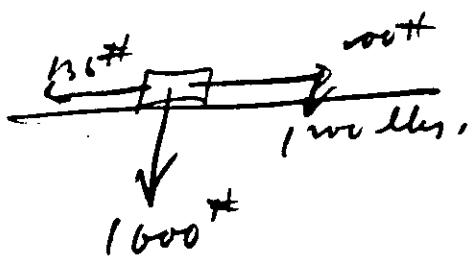
~~should be~~
~~should be~~
is then heated with ~~NH_4~~
a slight excess formic acid
 $[\text{Cu}(\text{NH}_4)_2\text{WO}_4]$ to remove
oxides of Cu as well as

CASE
301



$$\bar{x} = T \sin \theta - \underline{v}$$

$$\bar{y} = T \cos \theta - 1 = 0$$



$$f_n = 136\#$$

$a = ?$

$$\sqrt{1600 - 136} = \frac{1600}{3} a$$

$$a = 11.8 \text{ ft/sec}^2$$

$$F = \frac{1600}{3} \times \frac{36}{36} + 1600$$

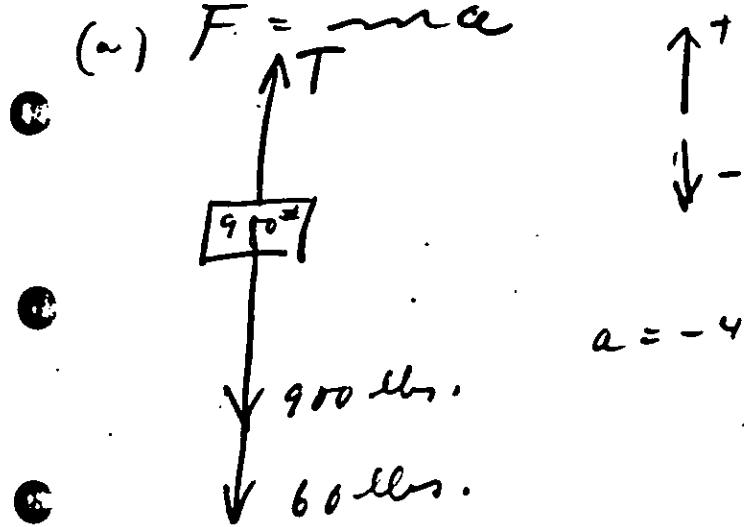
$= \sqrt{118}$ lbs. base
exc to roadbed

net weight on roadbed =

$\sqrt{1600} = 40$
 $\sqrt{118}$
1600 square & 40 roadbed

3/4/38

(a) $F = ma$



$$a = -4 \text{ ft/sec}^2$$

$$(T - 900 - 60) = \frac{900}{3}(-4)$$

$$T = -112.5 + 960$$

$$T = 847.5 \text{ lbs.}$$

uniform velocity upward

$$T - 900 - 60 = \frac{900}{3} \times 0$$
$$T = 960 \text{ lbs.}$$

uniform velocity downward

$$T - 900 + 60 = 840$$

$$W = 1600$$

$$m = 160$$

$$w_0 = 4 \text{ ft/sec}$$

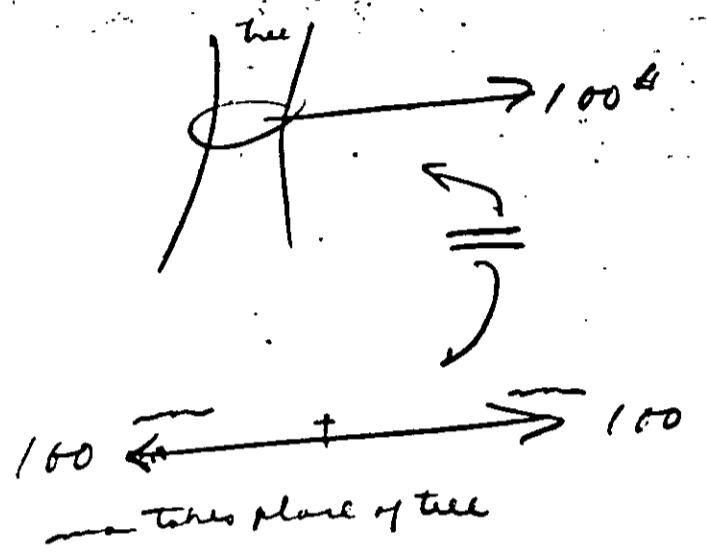
$$t = \sqrt{rc}$$

$$\frac{m}{T} = \frac{0}{T}$$

$$a = +\frac{4}{T} = 4 \text{ ft/sec}$$

$$f = m$$

$$T - 1760 = \frac{1760}{3v} \text{ sec}$$



newtons third law - to every action
there is an equal reaction
so big forces occur in pairs -

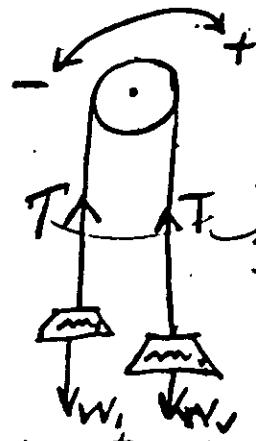
$$\text{get } \begin{cases} F = ma \\ W = mg \end{cases}$$

If mass is in lbs. weight will
be in pounds

If mass is in slugs. weight will
be in lbs.

part 1 - 31-13

Q. How is the centripetal force in the pull of the earth on a 1 gm. mass.
(Radius of Earth =
arc. of $\theta = 970 \text{ cm/sec}$)



- Q. accelerations are equal
cover up to dia gram & deal with
1 part
- Q. acceleration of gravity & Centrifugal force
not be

$f_a = m a_{\text{cent}}$
cancel
charge of e .
 m

$$T - W = m a$$

$$T - W = m a$$

3/4/3 ✓

① Na_2CO_3
nuret B

H-50y
nuret A

$R_1 = 0.00$
 $R_v = 34.39$
 $R_c = 34.40$

$R_L = 0.07$
 $R_v = 34.45$
 $R_c = 34.30$

② Na_2CO_3
nuret B
 $R_1 = 0.00$
 $R_v = 33.14$
 $R_c = 33.15$

H-50y
nuret A
 $R_1 = 3.76$
 $R_v = 41.90$
 $R_c = 32.86$

3/11/39

(1) Na_2CO_3

$R_1 = 0.00$

$R_v = 33.83$

$R_c = 33.84$

$H = 504$

$R_1 = 0.00$

$R_v = 33.28$

$R_c = 33.65$

(2)

$R_1 = 0.00$

$R_v = 31.40$

$R_c = 31.40$

$R_1 = 0.00$

$R_v = 31.38$

$R_c = 31.23$

66.50
6.80

~12512 v. w.g #1

R_v

~~4.10~~
~~5.14~~

~~1.37~~
~~5.14~~
- 8,000 v

R_v

3.5485

~1650 v

6.1988

R_s

Papel

ellen + $\frac{140}{1000}$ = ~51.99 g.

ellen - $\frac{140}{1000}$ = 15 v. 00

99.99 g.

.3 v

~v.096 100.31 g.

ellen dry = 9 v. 56 g.

ellen + $\frac{140}{1000}$ = 19 v. 39 g.

19.39 v. 26

$19.39^{\circ}\text{C} = 7.89 \text{ m}$

3/13/

$$\begin{array}{r} 19.539 \\ \hline 99.83 \\ + 1.58 \\ \hline 100.41 \end{array}$$

#1 ^{initial} R₁
R = 33.07 m. Nevco
R₂ = 0.00
~~R₃ = 33.05~~ R₃ = 33.08 | R₄ = 1.62
R₅ = 32.55
R₆ = 21.55

#2 R₁ = 0.06
R₂ = 34.06
R₃ = 34.01 | R₄ = 1.02
R₅ = 32.54
R₆ = 32.44

~~34.06~~ - 33.54
- 1.62 1.02

31.63 - .09 32.54

21.55 .08

21.44

6.650
6.000

Silica will be examined for
contaminating constituents.
 SiO_2 should be perfectly white
in color.

b6 b7c

avoid hydrolysis.

H₂TiO₃ might have some
Fe & it will be colored. Then
have to resort to a visual
fusion.

Filter out H₂TiO₃ and
from boiling hot soln
wash with A 1+D, isolate
isolate to Ti⁴⁺ & might
precipitate

Take paint pigment which
is good resistant.

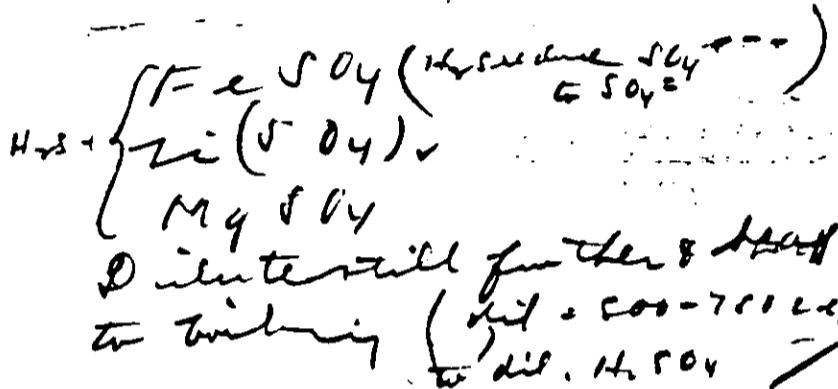
/ precipitate Fe corross and
dry H₂TiO₃ & precip Fe by

NH₃. Ignite Fe to Fe₂O₃
& = filtrate precip Ti⁴⁺ as

1/4 g NH₄PO₄ precipitate to
Ti⁴⁺ & H₂O₂

H₂TiO₃ might cling to
vessel ~~and~~ walls. Best to
dis in A cone, H₂-S₈
& dilute & rehydrolyze
again.

mid of Pt. latheate sol.
with H₂S → brown
Pt S_x (stall in cold).



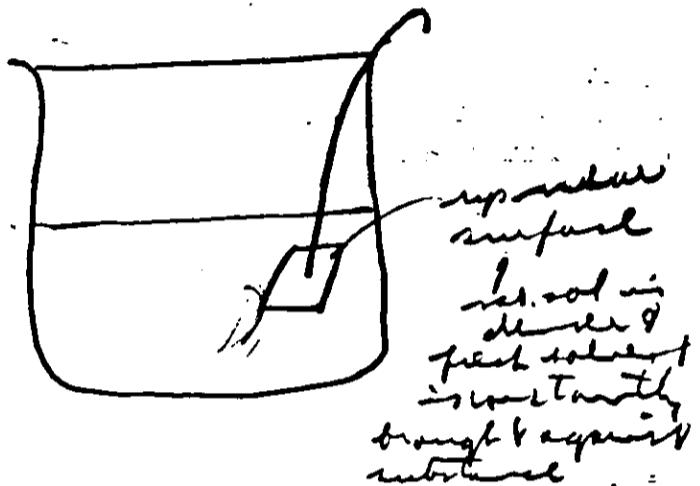
Prepare a strong sol of NaClO,
add it carefully dropwise
to above, as drop by drop,
get FeS & as the FeS dissolves
& & continue until a drop or
two one would produce a
permanently greenish of FeS.

In other words, heat
[H⁺] to just enough to keep Fe in
sol.

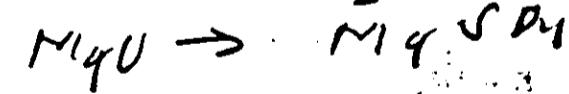
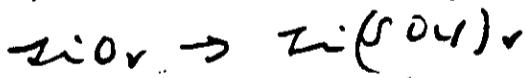
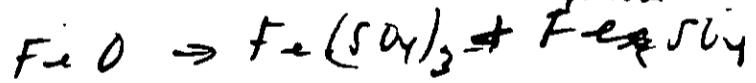
Heat not to boiling while
still passing H₂S thru sol.
in carbon flask. If H₂TiO₃
will separate as white ppt,
miss. Ferric is a
FeSO₄ + Mg as MgSO₄.

Purpose of keeping Fe in
ferrous condition is to

gently to move, & are able
to lift it almost all out.



• cover melt bath w/ SiO_2 , &
• then bring in Pt wire etc.
Allow to dissolve in cold



very faint at CaO
weak & old

KHSO_4 acts on Pt, etc. to get

TiO_2 = Rutile

Procedure - 5 g ~~sample~~ or
 $KHSO_4$ (comes highly hydrated)

$\sqrt{KHSO_4}$ + water of approx $\xrightarrow{\Delta}$ fluid

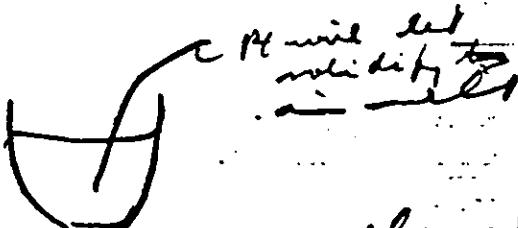
+ bubbling & spattering $\xrightarrow{\Delta}$ just

drive off H_2O $\xrightarrow{\Delta}$ (K_2SO_4)

spattering + H_2O $\xrightarrow{\Delta}$ $K_2SO_4 + SO_2$

• end of regularity
do the work
of converting
constituents into
sulfates.

First get to $\frac{1}{2}$ vol,
then introduce
weighed sample & heat
just a little on the & decompose
will be readily & efficiently
accomplished, keep over
covered & watch it carefully
silica will float around in white
flakes & mineral if undecomposed
will be dark. Allow to cool



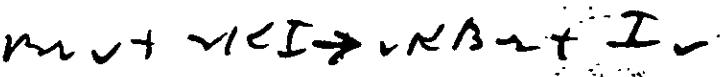
Then apply boric glaze

3/13/38 wed.

Dr. Baker

Estimation of Titanium

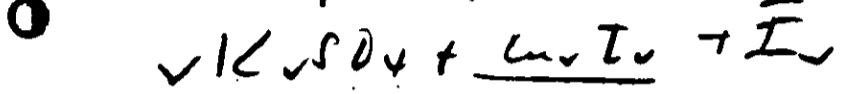
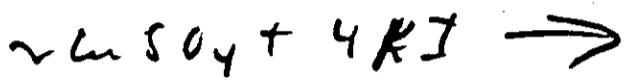
- ① p. 108, 115, 116, 114, 150,
156, 160, 549A, 597 & H
- ② where Ti would appear in a
qualitative examination.
Ti not a first group - no chlorides
- ③ Ti in third group. NH₃ lowers
[H⁺] of solution & get hydrolysis
or precip H₂TiO₃. ∵ Get
white gelatinous precip
- ④ sol. acid which might
be mistaken for Ti.
H₂TiO₃ might be mistaken for
silica. (in ores & minerals)
- ∴ to get Ti bearing ores into
sol.
- ⑤ ~~proceed according to~~ proceed
use for example ~~Manganite~~
 FeTiO_3
 $\text{FeO} + \text{TiO}_2$ ilmenite



(✓) ρ_{M} of iodate

- o $1\text{KI O}_3 + 5\text{KCl} + 6\text{HCl} \rightarrow$
 $6\text{KCl} + 3\text{H}_2\text{O} + 3\text{I}_2$
titrate with $\text{Na}_2\text{S}_2\text{O}_3$. This
- o gives I_2 for 1 mole KI O_3 .

number of acids present
in dilute



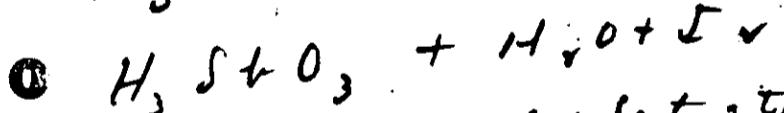
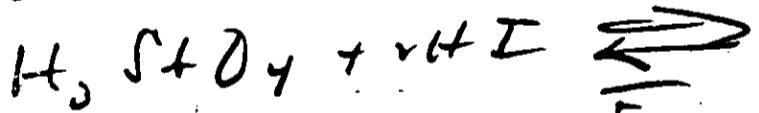
still & liberate I₂ into

I₂ or Cu₂I₂ gives color
to starch.

6. Det of Pb.
by H₂I.

Pb often alloyed with Pt
& sometimes Cu - Pb bangles

Pb.
Pb in higher state of oxidation
reduced by H₂I + I₂ is
liberated & det. as usual

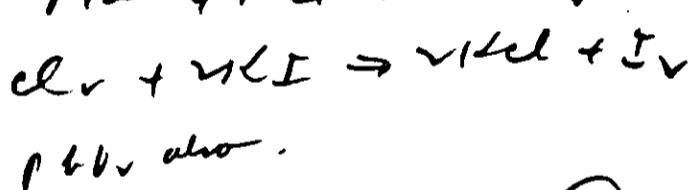
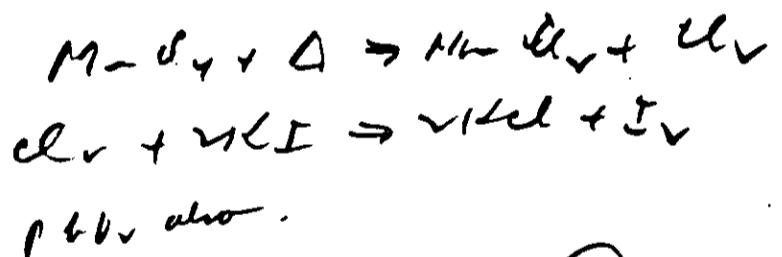
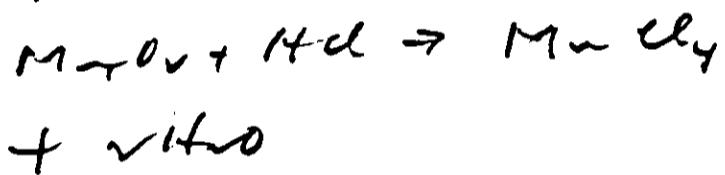


In presence of soluble tartrates
preventing formation of their
salts in similar reaction can
be carried out without distillation
of I₂.
Have the other air salt
in presence of tartrate & excess
Na₂S₂O₃.

Details see text,

7. H_3AsO_4 may also be reduced by H_2 .

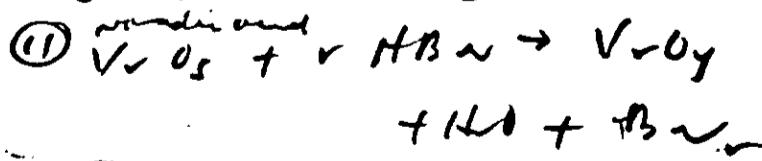
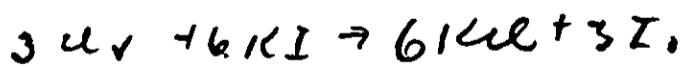
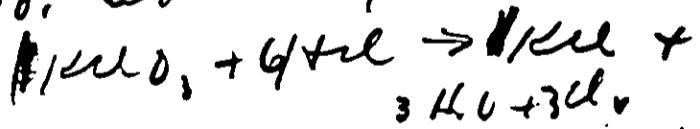
8. M and (pyrolytic) decomposing liberating Cl^- (from HCl) + conduct in KI sol & Cl^- will liberate into equivalents of Cl^- .



p 60° also.

9. B_2 , est. as B_2 . in ③

10. Reduction of chlorates



c.c. titrate with $\text{Na}_2\text{S}_2\text{O}_3$
adding start toward end.

3 KI does not have to be accurately weighed out as long as we take excess.

Part - dark brown layers oxidized

14 E

addition to a white
part std. I - by H_2O_2 weighed
out.

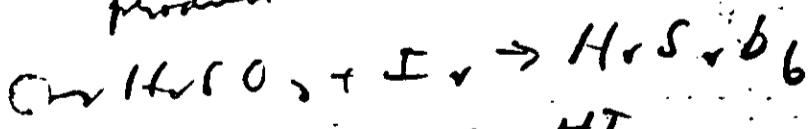
Applications of std. I - solution
used in oxidation reactions

① As add with Na_2WO_4

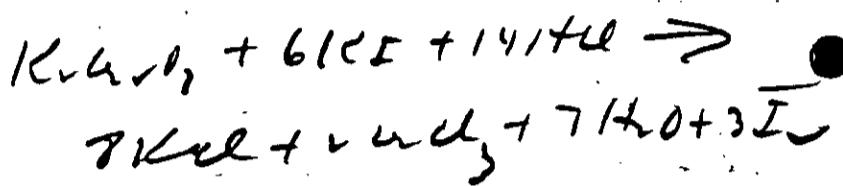
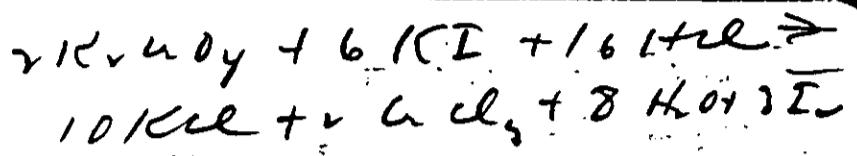
② $\text{Na}_2\text{S}_2\text{O}_3$

③ Sb - sol. add with NaClO_4 ,
should form tetrachlorate to
form complex with Sb &
prevent oxidation of Sb.

④ SO_4^{2-} may be determined only
when $[\text{H}^+]$ is low otherwise
dithionite and may be the
product instead of the SO_4^{2-} .

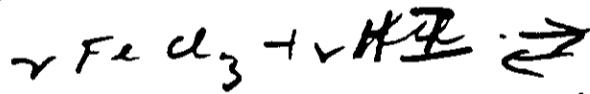


∴ It would appear to be
greener.



get chrome salt green or
violet & I₂ quite different
recognizing end point. Best to
use both solutions extremely
dilute. probably MnO₂ coating
on AgI is sol. of K₃FeO₄ makes
colorless (investigate?). Changes
from deep green to colorless.

4. Test of Fe



$\sim \text{HCl} + \sim \text{FeCl}_2 + \text{I}_2$
easily removable. It is
advisable to distill iodine
from sol. into KI & then
titrate I₂ with Na₂S₂O₃.

5. Copper salt with iodide (such application)

conducted in presence of
free H₄I₄, H₂I₂, & H₂H₂O₂. If I₂ is distilled & not
in distillate - otherwise

6.6%
6.8%

Sec. - 10910 - Mar

Applications of Solvothermic processes

Two types

- ① I (class) one diss in KI
ants or use of drying agent
o I inhibited

Process

- 1. Process of extraction of gold
Brown

- Caustic Na₂ to come in contact
with excess KI

Chemical

- Ba_n + nK⁺I⁻ \rightarrow nKI + Ba

Other

- & del I⁻ by $\text{Na}_2\text{S}_2\text{O}_3$,
many time other things with
no water and ~~water~~ do
not dissolve off into
Ba_n is dissolved off into
+ KI bulb + titrate a titer
is made directly in
receiving vessel

Chemical

- 2. Cl₂ (same as Ba_n)

Other

- Carry out both of above reactions
in acid solution.

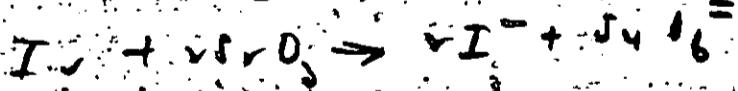
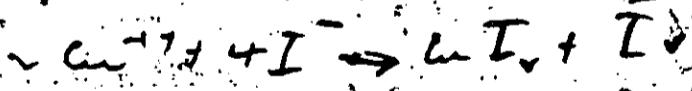
Other

- 3. lot of Cr in presence of
free acidic while in higher
state of oxidation.

and this can nitric acid
and Na_2SO_4 . but not
to remove NO_2^+

Add Br_2 water at end &
but oft Br_2 to make more all.
 NO has been driven off.

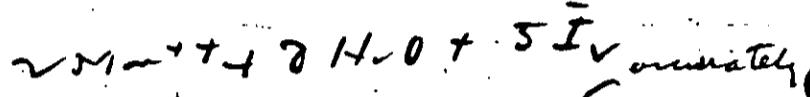
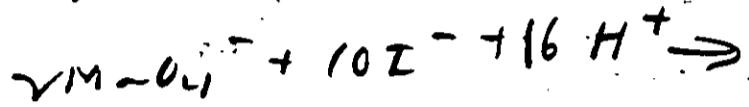
- boil of excess of NH_3 &
add HgO to diss any
 $\text{Cu}(\text{OH})_2$ which may resp.
& then the sol. may
contain $\text{Cu}(\text{NH}_3)_4(\text{NO}_3)_2$.
- bring to interest with
about 3 g. KI . It will
be titrated. Run in $\text{Na}_2\text{S}_2\text{O}_3$
not until I_2 is almost but
not entirely consumed. Then
add starch paste & complete
titration to colorless
- little last remains in
sol: a faint blue color due to
addition of starch may remain
after end point.



A std. sol. of $\text{K}_2\text{Cr}_2\text{O}_7$ sol.
may be used instead of KI .

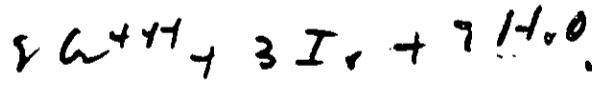
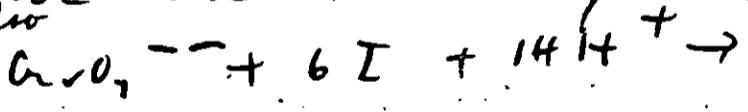
200 μ l of 0.05 N KI added to 20 ml
and vol. of KI

~~KI + I₂~~



add a vol. of 25-40 ml. 0.1 N
KI to 50 ml. H₂O in
a cuvette a vol. of 80 ml.
of 12% containing 2 g I₂ &
5 ml of conc. HCl, the
mixture should then be
placed in the dark for
2-5 min & dil to 300 ml.

titrate with Na₂S₂O₃ to
be standardised.



add 10 ml. K₂Cr₂O₇ by direct
weighing out.

5-10 ml of 12% H₂O₂ run into beaker
add 5 ml KI + 2 ml. H₂O & 10 ml.
conc. HCl & allow to
rest in dark, dil to 200 ml.

Dilute to 10 cc. a trace
with standard K₂S₂O₈ to
the appearance of a
violet blue color then
running unchanged
or further addition of
oxidizing agent, or no
addition of K₂S₂O₈ until
0.5 cc. white - the
amount of 1 N K₂S₂O₈
necessary to oxidize the
indicator, calc. 3.0 F. &
from sample.

9.0

pls
see

- 2 - Bureau of mines
- 3 - Dept of materials
- 4 - Treasury Dept
- 5 - Geological Survey
- 6 - Reports of

Estimation of production costs

* Profits

- 1. Rechart p. 61~~g~~
- a - people lost money when a scientific study would have shown how hopeless their operation was
- we need to rethink

* expenses

- a - work on research from economic side
- get Weiss & Cross book.
- points out sales dep to date
- b - demand
- ** what yield can be expected as basis for cost estimates
- i. careful analysis of costs of new plant before starting plant
- ii. make and get
- 3. Diff' bet dem cost &
~~1. part of plant~~
- 1. costs higher in field plant

p. 66 & 67

+ less forward at

est. costs for all capacities besides

normal

not couple of hours development

market surveys

1. demand analysis

a - Dept. of Commerce bulletin

b - Bureau of Census

3/10/3 ✓

Market Develop &
Reproduction Financing

Gaining new Capital
methods

- 1. Sale of additional
capital stock

In order to do it must have
organization already
set up

- 2. Long term loans or
stocks.

also needs long established
company, too

- 3. Short term loans - not as
good as they may be
~~as~~ called.

- 4. Financing from surplus
as well to have already
well organized organization

Pros & Cons

Problems in Research
present ordinarily classified as
overhead & usually first to go in
depressions

Laboratory is ordinarily a
service bureau

- 1. Can eliminate costs by keeping
amount of borrowing

depts & how much you have helped.

not always possible to do this as a little testing often do a great service.

i record every analysis & show how much each analysis would cost outside

Development Dept.

and get last years costs & estimate this years & what they can bore for in way of a return. If we finished anything the estimate its value & start.

summary : you may know value of your dept but many does not unless you put it down in black & white.

Working Development Problem.

1. personnel necessary
2. time for completion
3. no of workers

"App & man
1. Value of Product

Items for overall Budget

1. Direct salaries & Direct labor
2. Job. Equip
3. materials & supplies
4. salaries for director & supervisor
5. Indirect salaries & labor
6. light, Heat, Power
7. telephone, Painting, postage

6.6.60
6.6.60

7. Fuel Expenses

8. merchandise dues

9. Bonus & special compensation

10. Insurance

11. Rent for building & tools

12. Tax & administration

overhead.

13. Total Plant Expense

14. Miscellaneous Expense

fixed expenses

variable all expenses

1. Any improvements of

existing process

a. reduce cost of operation

b. improve Q. quality of

product.

2. Developed new uses for

existing products.

3. Developed entire new

process

a. old product

b. New product

4. Product sales

a. Set out to organization

b. sell pattern or blueprint

5. Supplies ideas for sales

or organization

6. "Year of Research Idea"

Intangible things tend to analyze

1. Helps customers & breeds
good will.

next Patients
in week

66.50

not known or used by
others in this country before
his invention, or
or not patented or described
in any printed publication
in this country or in
foreign country before
his invention or discovery
thereof, or more than
two years prior to his
application, unless the
same is proved to have
been abandoned, may
upon payment of the
fees required by law,
& other due proceedings,
obtain a patent therefor.

a patent is contrahable between
parties
i. Inventor - Retainorship
ii. Public (Gov.) - This idea to
public.

at the end of several years.
right ceases & only by special
act of Congress can it be renewed

Obtain Patents on

- i. Art
- ii. Machines
- iii. Compounds or composition of matter
- iv. Designs

3/11/38

Off right - Inventions &
Patents (library)

● Reasons - Chemical Patents

1992 - Patent 6,000,000

1911 - " 1,000,000

1984 - " 1,800,000

5,000,000 patents in US. give 1,000,000 a year
85% of industrial output is
protected by patents

● Why want a Patent

1. Can keep it secret

a. more labor intensive

b. Integrity of workers

c. Closed at opt (keep people out)

d. Somebody else might get same idea

2. Can file Patent

1. Have to publish whole idea

2. Gain monopoly for
years that patent runs

See 3. art 1. Patent Law

1. Economic to public

a. to profit it invents

Any who has made or
discovered any new & useful
art, machine, manufacture,
or composition of matter,
(chemicals)

or any new & useful
improvement there off.

29/11/34

Chap II

Developments of Ch. C. Projects

1. Research Laboratory

Want to know if

i. Basic ideas are sound

ii. Is it attractive economically

1. Economics. (It must be avoidable after the basic developed in idea/pattern patent I should search all patent literature.)

2. (a) All potential markets exists

(b) Peculiar characteristics with respect to distribution.

a. Regions

1. Conduct "consumers test"

(d) Financial Risk

1. i. must develop step by step

ii. must have ample capital available before starting

iii. losses must not

iv. however losses can be

by other concern who developed fully

v. now a budget before each step

vi. have accounting department & estimate expense

(e) Have experimental dept entirely separate from

rest of plant

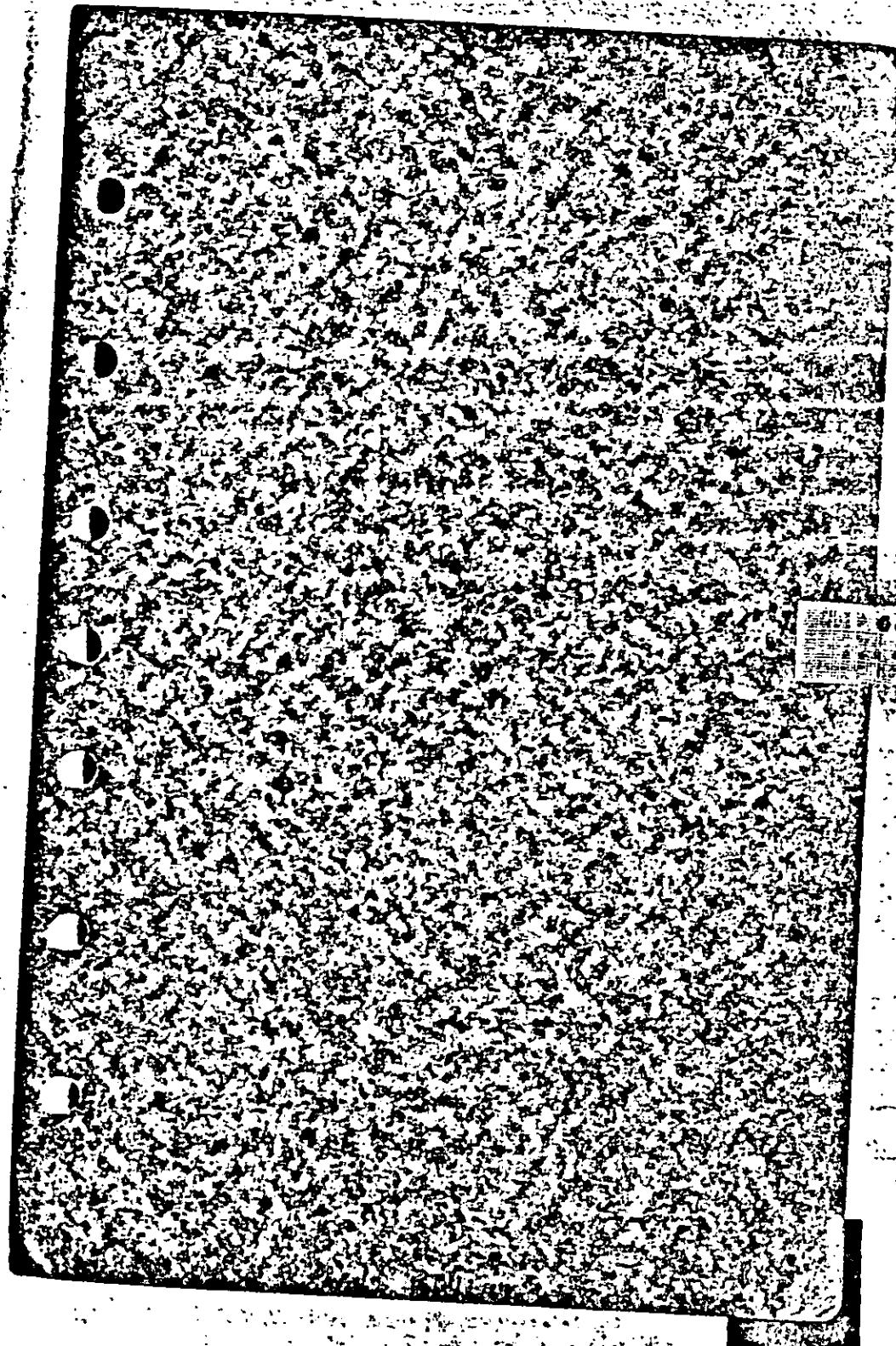
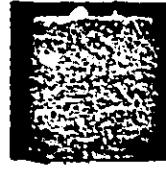
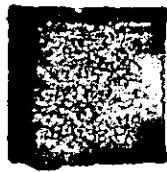
Principles of Tech Development

1. Research usually carried out first
in, small laboratory brief
then it is carried out into
plant by chem. engineers
2. Development
3. Full scale trial object

method for Ch.E. Process development

1. Relation on laboratory scale
2. Large batch operation
3. Large single unit
 - a - Design of apparatus
 - (i) not associated to cost
 - b - Knowledge of Design
 - (i) design - turning device into design / first
was had to design at
 - (ii) need large organization for
specialists in a - b -
then evaluations or to materials
 - c - Draw conclusions or to materials
of construction & design
4. Semi - commercial plant
(different works)
 - i. ought not to seriously short
important details
5. Pilot plant (commercial plant)

6.5 ft
6.5 ft



- p.30
- aufziehen, a, s, to paint
die Wachtstube - m, guard-room
das Bildentwurf - es - er, guild hall
Angefühl, approximate
das Standbild - es - er, statue
vergoldet, gilded
das Zepter - s - scep^ter
die Weltkugel - m, globe
erraten, ie, a,
der Dom - es - e, cathedral
der Kaiserstuhl - s - e, imperial throne
niedemessen, ie, ie, to tear down
bedeutungsvoller, portentious
abbrechen, a, o, to tear down
die Kuppelkammer - m, bower
die Merkwürdigkeit - es, curiosity
aufstellen, to place as new, exhibit
die Glasmalerei - es, stained glass
p.31 das Gemälde - m, painting
ferner, furthermore
Heidnick - heathen
der Opferaltar - s - e, sacrificial altar
merckig, foul coward
die Sack - m, sack, box
die Coryatide - -, coryatid
gedreht, crooking, bending down
stützen, to support
unfreundlich, unpleasant
 hässlich, ugly
das Kind - s - er, fool
ein Kind schulden, to owe
in demen, however
der Christuskopf - es - er, head of Christ
der Dom - s - m, thor^o
fröhlich, to be merr^e, indeed

C.2
misterhaft, mysterious
das Mysterium - - s, death
gott geboren, born of God.
der Kieland - - e, savio.
das Leid - - s -, suffering
Leidenschaft, to lead into
error rather
der Leidenschaft - - - alle, lecture. soon
der Lusthof - es "e, amir, total
der Lust - - - l, last
überflüssig, impetuous
langweilig, tedious
erlösen, to save, rescue
wo? - - - where, by what means? why?
how? when?
abgetragen, worn out
hervortreten, to appear
erwerben, a., o, to acquire

C.3
die Vaterstadt - "e, native town
das Elbelgräbnis - res - se, faintly only
aufgeklärt, enlightened, rationality
geistig, immaterial
schriftlich, in writing, in black
und weiß, in white
unheimlich, mysterious
süßlich, sly, cunning
stümmerlich, thick
das Augelein - "e, little eye
verblassen, dim
angstlich, fearfully, timidly
sich will - - - great dolor, I didn't
der Kirchhof - es "e, churchyard
ordentlich, regular
streiten, i., i., to strike

- ^{p. 34}
smithaft, solange, никогда
der Bart - es "e., beard
blider Chorale gal, as for the Chorale
die Lust, joy, pleasure
die Ruhelosigkeit - n., restlessness
manierlich, refined
die Heigl - n., violin
verziert, to decorate
das Lutterwerk - s., lattice work
das Porzellanfigürchen - s., little
porcelain figure
der Stetyl - s., bat.
bunt, varicolored
des Leidenschafts - es - e, sick stuff
künstlich, artificial
ansprechen, a., o., to appeal to
desto, alle (with comparatives),
das Lorbeerblattföfen - s., little laurel
^{p. 35}
blätter ausdrucken, to look out
des Parterrefenster - s., ground-
floor window
das Glockenblumchen - s., bell
flower
(1) artig, pretty
die Grätzle - n., cap
kümmern (sich) to care, bother
aufgerissen, gaping
des Maul - s - er, mouth(gape)
(1) vereitert, petrified
das Kloßauge - s - -, google eye
qualifiziert, pretty
der Diebstahl - s - e, larceny
bold, fair, dandy

6.50
C. 13) zunächst für den, to rest back
das Antlitz - es - e, countenance
genau, detailed
durchdringig, clear
die Deckkörnung - er, embossed
der Donnerabenddach - es - e, summer
evening bough
der Fruchtigallentaut - es - e, song of
nightingales
der Rauchduft - es - e, scent of smoke
der Haupthof - es - e, corridor
rauh, quick
entfliehen, o, o, to escape
verschlichtigend, conciliatory
geheiratet, snub
der Wiedereinsatz - es - e, resumption
entblättert, unconvincing
die Zauberformel - er, magic formula
C. 14) Schmiede & Lieblichkeit, formular
of their mouthed
begingen, a, us, to conquer
das Dorf - -, a town, lodgings
gewähren, to give, afford
gärfri, to sweep along
das Ross - es - e, steed, charger
die schwel - -, smoulder
das Wasser auf spülen - s, washing
die übrigern, all rest of
der Unheil - es - e, evil, mischief
mit Mutter zugesetzt, sealed up with boar's
durchbrechen, to break through
riesig, gigantic
der Peter schüssel - t - , St. Peter's key
die Unsterblichkeit, immortality
aufschneiden, to open

p. 34
der Spießbürger - a -, citizen
die mortenkästchen - or, night cap
die Trappfalle - or, clay pot
das Maul - s - u, mouth (of animals)

- leise, muted
behaglich, comfortable
das Lebensatmosphäre - a -, spark of life
dinner vegetarier, to vegetate into
● der Geograph - er - er, geographer
● verlegen, to change the position of
schmeichelhaft, flattering, coquettish
duftend, to be fragrant
das Sonnenblümchen - eins - eins, sunflower
ambivalent, ambivalence
● ein tiefes Fühl - fuhl - more intensely.
wirring versteckt, with charming shyness
umhüllen, to envelop
ausdehnen, to breathe forth
● erzählen, to show
die Leichtigkeit - en, bliss
leben, to tremble, quiver
die Stimmung - u, mood
● aufschlagen, to open
schimmernd, to gleam, glister
einer syphon, amoral
schwul, to pack
der Raupe - a -, caterpillar
● bringen, quobachte, zugelassen, to open
selbstlos, through
begegnen, to happen to
der Angst - " o, fear, terror
der Heist - es - er, heist
● der Österreichische Beobachter, the Austrian observer
der Verstand - es, reason
des Herzens - s - es, soul
zufällig, accidental
behaupten, to maintain, assert
der Verhandlungsschluss - de - e, process
of recovering

- P. 36
- die Vorausfrage, forecast
fortwährend, continually
der Vorsprung - es \ddot{u} e, excellence, advantage
pflegen, to be accustomed
abstrakt, abstract
transzendent, gray beyond belief
der Leidrock - s \ddot{u} l, coat
schröff, harsh; angular
gerade (gerade), straight
streben, to strive
soziale positive
sehrlich, fine, splendid
das Christentum - s, Christianity
die Broschüre - m, pamphlet
die Unverantwortlichkeit, irrationality
die Verhältnisbarkeit, reversibility
überhaupt, in fact
die Menge - m, quantity
die Vortrefflichkeit - er, excellence
recommenden, to boast
ernsthaft, serious, solemn
die Herricht - er, regard, respect
die Achtung, esteem
verdienen, to deserve
erstellen, to consist
der Hauptpunkt - es \ddot{u} e, most part of the
aber, just
einst, once upon a time
der Bediente - m - m, servant
ausüben, to exercise
beschwichtigend, conciliatory
in derse, however
entsetzlich, terrible
die Darstellung - er, portrayal
das Grauen, terror
aufzustellen, to find a cold shiver
durchzittern, to shiver through

2.3

auch, besides
ergänzen to complement, provide

absichtlich, intentional

besonders, especially

größtlich, large

getragen (mit), to bear

der Glück - s - e, spot

unwillkürlich, involuntarily
über dies, beiold, more over

C zuwidrig, disagree

unterstreichen, underlined

aufrichtig (mit), to sit up

erblieben, to persist

unterhaltlich, entertaining

O schwerfällig, ponderous

gähnen, to yawn

und, well, and that too

C volle, full

unterdrückt, meanwhile

verfließen, to elapse

von vorn, from the beginning

O heifed, scaldingly

hell, gellend, shrill

ärgelich, vexed

die Heratterin - er, gossip

C schlottern, to shudder

schlappen, to drug, twiddle

mitteln; to run

das mark - s, marrow

das Eselhaut - es, asper leaf

C wagger to dare

das Desperat - es - ei, ghost

C zusammenknipf, to pinch together

der aufgekleis - es - e, orbit (of the eye)

das paradiesches Röhrchen, bamboo cane

stützen, to support

c. 39
mundfaul, slow, drawling
die Türröhre - er, illusion
die Phantäse - er, imagination
die Bedingung - er, condition
der Abschnitt - s - e, section
das Hauptstück - es - e, chapter
also daas, then, elsewhere
der Klepperkugelball - an, belgie football
problematisch, hypothetical
der Logogrymus - , - er, slogan
der Beweis - es - e, proof
durchaus keine, no . . . at all
klapperig, to chatter
die Kärtchentafette - n, cartouche
die Leidensangst " e, mortal terror
unbedingt, unconditional
der Satz - es " e, proposition
spukhaft, ghouly
die Abneigung - er, aversion
das Herze wohlb, roundabout
die Absicht - en, purpose
c. 40
der Engel - 1 -, till
der Nebel - 1 -, fog, mist
verschwinden, to disappear
schwärmen, to swarm
der Nachtmarsch - s " , night march
die Tasse - n, cup
mitteln, to share
der Schlaf - es, sleep
das Bleid - es - er (al.) figure
grünen, to green (the hair), will
die Petroneide - n, matin
das Wiesental - es t ev, meadow
blitzend, to sparkle

p. 13

tray, in spite of
unpleasant, enormous
Kante, f., edge

wormholes, to surpass

(1) Anzahl, f., number
verhindern, to prevent
Verfinsternung, f., eclipse

① Reduzierung, limitation
exceeded, considerable

(2) XI

Kreis, m., top

als beweisen anzuhören, except as
proved.

② best - with sufficient, consider-

requisites, notwithstanding

Gegenstand, m., object

verhindern, to cause
wonderfully, to fly past

genau, exactly

entgegengesetzter, opposite

③ als die ist, from that

ander, however

billig, m., conclusion

ausführbar, applicable

c. 15 XII

Schwere, f., gravity

Gewicht, m., weight

Aufzugskraft, f., force of a traction

Folge, f., result

Abwurfkraft, f., force of gravity

beschleunigen, to accelerate

beschleunigt, m.; all other hand

beschleunigen, to cause

- c. 15 **beginning**, f., designation
C. eng. - verb, the closely connected
Vorstellung, f., conception
Seil, n., rope
bewirken, to produce
ziehen, to attract
④ **ber** - - Körper, with the mutually
attracting bodies
unwahr, invisible
vorhanden, present
① **Greise** - - deproliferator, moreover, and
is spoken of as a force
fortwährend, continuous
e. 16 förfallen, to push
Ringknoten, n., knot
④ **dadurch** - das - wifft, by pushing down
⑤ **wickeln** - - windet, refers to
Rütteln, to support
④ **nach - zu**, towards
④ **wird** - angreift, is invaded
④ **vehicle** - - von which is excited
independently of
natural stand, n., natural object
zugänglich, a visible
the tractable, actually
naturwissenschaft, f., natural science
Hauptpunkt, n., chief point
verhafft, to secure
natürigkeit, - ; natural law
wonach, according to which
④ **stetig** - - - - - - - - - - - - - - - - - -
gradually, any two whatever
connected, mutually
allmählich, gradual

~~Nov 10, 1958~~

~~Hole - German Short Stories
Edition 1951~~

Sec. 3

p. v 3 & ~4

6 th exercise

1st & 2nd sentences

p. v 5
Adverb & phrases for
review
writing

Porterfield - German
short stories

~~Sec. p. 30 l. 6~~
~~p. 33 l. 14~~

~~+ last~~
~~of 33/35 now~~

~~dictation~~
~~dictate assistance~~
~~sentences~~

$$I = \int y - a(-x+1)^{\frac{1}{2}} dy$$

$$\textcircled{1} \int (\sin ax)^m (\cos bx)^n dx$$

$$u = \quad dv = \dots$$

$$\textcircled{2} = \int \frac{(\sin ax)^m (\cos bx)^{n-1} \cos bx dx}{uv}$$

$$\textcircled{3} \int x^m x^n dx$$

ans. for 21 ed.

Chapt III

art 137
139
140

p. 231 $\textcircled{1}(b), (c), (d), (e)$
 $\textcircled{2}(a), (c), (d), (e)$

1.2.5

⑤, ⑩, ⑯,

1.2.5, ③, a+b.

$$⑤ \int \sqrt{a^2 - x^2} dx$$

$$\left\{ \begin{array}{l} u = \sqrt{a^2 - x^2} \quad du = dx \\ du = \frac{-x dx}{\sqrt{a^2 - x^2}} \quad u = x \end{array} \right.$$

$$= x \sqrt{a^2 - x^2} + \int \frac{-x \cancel{dx}}{\sqrt{a^2 - x^2}}$$

$$I = -x \sqrt{a^2 - x^2} - \int \sqrt{a^2 - x^2} dx \quad I$$

$$+ a^2 \int \frac{dx}{\sqrt{a^2 - x^2}}$$

$$2I = -x \sqrt{a^2 - x^2} + a^2 \arcsin \frac{x}{a}$$

$$I = \frac{1}{2} \sqrt{a^2 - x^2} + \frac{a^2}{2} \arcsin \frac{x}{a}$$

6.6.80

mon. v 118/3 v

art 1~6 review 0-71

" 1~7
" 1~8

① review formulas
on p. 191, 192 to 13 in.

① art 1~9
practice off - n. 195

(10) ?
(11) ✓
(15) ✓

p. 196

(18) ?

(~0) ✓

(~7) ✓

(~8) ✓

(~9) ✓

(33) ✓

But what we mean to find is
a function when the derivative
is given

then

$$\frac{dy}{dx} = f(x) \quad (1)$$

Find y

$$\frac{dy}{dx} = \frac{x^v}{y}$$

cannot find y by elementary fits.

$$y = \int f(v) dv \quad (2)$$

$$dy = f(v) dv \quad (3)$$

(1), (2), & (3) are all identical

$$y = \int v^v dv$$

$$\frac{dy}{dt} = vv$$

$$dy = vv dv$$

$$y = v^v$$

$$y = v^v + C$$

6.6.50
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$$\begin{aligned} F_1(v) &= \int f(y) dy \\ F_v(x) &= \int f(y) dy \end{aligned}$$

O show $F_1(v) - F_v(v) = C$

O $\frac{dF_1}{dv} = f(v) \quad \left| \begin{array}{l} \frac{dF_1(v)}{dx} = \frac{dF_v(v)}{dx} = 0 \\ \frac{dF_v}{dv} = f(v) \quad \left| \frac{d(F_1 - F_v)}{dv} = 0 \right. \end{array} \right.$

O this is only possible when
 $F_1 - F_v \equiv 0$ Q.E.D.

O \int - indefinite integral to show
 and there are any number
 of solutions

O $\frac{d}{dv} \left(\int f(y) dy \right) = f(v)$

O the derivative of an integral
 is $f(y)$ itself.

O $d \left(\int f(x) dx \right) = f(x) dx$

$$\int \left(\frac{dF(x)}{dx} \right) dx = F(x) + C$$

Table of Clever Integrals
(memorial)

$$\int x^n dx = \frac{x^{n+1}}{n+1} + C$$

(for $n = -1$)

$$\begin{aligned}\int x^{-1} dx &= \int \frac{dy}{y} = \log y + C \\ &= \log x + \log C = \log Cx\end{aligned}$$

$$\int \sin x dx = -\cos x + C$$

$$\int \cos x dx = \sin x + C$$

$$\int \sec^2 x dx = \tan x + C$$

$$\int \csc^2 x dx = -\cot x + C$$

$$\int \sec x \tan x dx = \sec x + C$$

$$\int \csc x \cot x dx = -\csc x + C$$

$$\int dx = x + C$$

6.65
2/20

$$\int \frac{dx}{x^r} = -\frac{1}{r} \frac{1}{x} + C$$

$$\bullet \int \cos ax dx = \frac{\sin ax}{a} + C$$

$$\int \frac{dx}{\sqrt{v}} = \sqrt{v} + C$$

$$\bullet \int a^x dx = \frac{a^x}{\log a} + C$$

$$\bullet \int \frac{dx}{\sqrt{1-x^2}} = \arcsin x + C$$

$$\bullet \int \frac{dx}{1+x^2} = \arctan x + C$$

• rules for elem. integration

$$(i) \int A f(x) dx = A \int f(x) dx$$

$$\bullet (ii) \int (f_1(x) \pm f_2(x)) dx = \int f_1(x) dx \pm \int f_2(x) dx + C$$

Illustrative Example

$$\begin{aligned} & \int \left(5x^3 - \frac{x^{12}}{3K^{11}} + \frac{1}{5} \sqrt[7]{x^5} - \sqrt{v} + \right. \\ & \quad \left. 3 \sin 5x + 7e^{-\frac{2}{3}x} + \frac{1}{\sqrt{y}} \right) dx \\ &= 5 \frac{x^8}{8} - \frac{1}{3} \frac{x^{-10}}{10} + \frac{1}{5} \frac{\sqrt[7]{x^7}}{7} \\ & \quad - \frac{1}{\sqrt{v}} v - \frac{3 \cos 5v}{5} + \frac{7e^{-\frac{2}{3}x}}{-\frac{2}{3}} \\ & \quad + \frac{1}{\sqrt{y}} \log v + C \end{aligned}$$

b.6.50
200

read $\sqrt{1-x^2}$

$$1-x^2 \text{ from } \\ p: 19x - 193$$

factor

$$\int \sin ax dx = -\frac{\cos ax}{a} + C$$

Table of Integrals

$$\int \frac{dx}{a^v + v^v}$$

If $a = \sec x$ we would have

$$\int \frac{dx}{a^v + v^v} = \arctan x$$

$$\therefore = \frac{1}{a^v} \int \frac{dx}{1 + (\frac{x}{a})^v} = \frac{1}{a^v} \int \frac{dx}{1 + (\frac{x}{a})^v}$$

$$= \frac{1}{a} \int \frac{d(\frac{x}{a})}{1 + (\frac{x}{a})^v}$$

$$\therefore \int \frac{dx}{a^2 + x^2} = \frac{1}{a} \arctan \frac{x}{a} + C$$

$$\int \frac{dx}{a^2 - x^2} = \frac{1}{a} \int \frac{dx}{1 - (\frac{x}{a})^2}$$

$$(\text{Now } \sqrt{a^2 - x^2} = \sqrt{a^2(1 - \frac{x^2}{a^2})})$$

$$\therefore \frac{a}{a} \int \frac{dx}{1 - (\frac{x}{a})^2} = \int \frac{dx}{1 - (\frac{x}{a})^2}$$

$$\int \frac{dx}{1 - (\frac{x}{a})^2} = \arcsin \frac{x}{a} + C$$

Derivation
formula 19 p. 192

$$\int \frac{dx}{x^2 - a^2}$$

now

$$\int \frac{dx}{x^2 + a^2} = \int \frac{dx}{x^2 + a^2}$$

$$= \log(x+a) + C$$

6.6.50
6.6.50

$$\int \frac{dx}{x-a} = \frac{1}{\sqrt{a}} \int \frac{\cancel{x-a}}{(x-a)(\sqrt{x+a})}$$

$$= \frac{1}{\sqrt{a}} \int \frac{(v+a) - (x-a)}{(x-a)(v+a)} dx$$

$$= \frac{1}{\sqrt{a}} \left[\int \frac{\cancel{v+a}}{(v-a)(\cancel{x+a})} dx \right] \cancel{du}$$

$$- \int \frac{x-a}{(\cancel{x+a})(x+a)} dx \quad]$$

$$\int \frac{dx}{x-a} = \frac{1}{\sqrt{a}} \log \frac{v-a}{\sqrt{a}} + C$$

Illustrative Example

$$\int \frac{dx}{3-x^2} = - \int \frac{dx}{x^2-3}$$

$$= - \frac{1}{\sqrt{3}} \log \frac{x-\sqrt{3}}{x+\sqrt{3}}$$

$$-\log a = \log \frac{1}{a}$$

$$\therefore \frac{1}{\sqrt{1-x^2}} \log \frac{x+\sqrt{1-x^2}}{x-\sqrt{1-x^2}}$$

as for 5.11

see 110 formulas

p 196 - 197 practice all
your time

$$\int (5x^3 - 7)^{-1} x^5 dx$$

$$u = 5x^3 - 7$$

$$du = 15x^2 dx$$

$$= \frac{1}{15} \int (5x^3 - 7)^{-1} (15x^2 dx)$$

$$= \frac{1}{15} \int u^{-1} du$$

$$= \frac{1}{15} \left[-\frac{1}{u} \right] + C$$

6.6.10
10

$$= \frac{1}{15} \frac{(5x^3 - 7)^{1/3}}{\sqrt{3}} + C$$

$$\int \frac{\cos \theta \cdot k \theta}{\sqrt{1 - \sin^2 \theta}}$$

$$u = \sin \theta \Rightarrow du = \cos \theta d\theta$$

$$= \int (\sin \theta)^{-1/2} d(\sin \theta)$$

$$= \frac{\sin^{-1/2} \theta}{1/2} + C$$

p. 197 all problems

74 $u = \log x$

$$\int \frac{u^v du}{v} = \frac{1}{v} u^v$$

$$= \frac{(\log x)^3}{3}$$

$$75 \quad u = e^x + v$$

$$\frac{\int (e^x + v)^3}{3}$$

ass wed

art 131

" 132

practic all integration
you can
195, 196, 197

all 199

p. 101, 102

table of integrals

$$\int \tan x \, dx = -\log |\cos x| + C$$
$$= C_1 \log \sec x + C$$

6.6.5
6/6/50

12-13

$$\int \tan x dx = \int \frac{\sec^2 x}{\sec x} dx$$

$$= \log \sec x + C$$

built up by mult. by
- 1

$$\int \sec x dx = \int \frac{\sec x (\sec x + \tan x)}{\sec x + \tan x} dx$$

the ~~sec~~ is different of
~~tan~~

$$\log(\sec x + \tan x)$$

(11) P. 103

$$\int \frac{dx}{1 - \cos x} = \int \frac{(1 + \cos x) dx}{(1 - \cos x)(1 + \cos x)}$$

$$= \int \frac{1}{\sin^2 x} - \int \frac{\cos x}{\sin^2 x} dx$$

$$\frac{\sin^2 x - 1}{\cos^2 x} = -\frac{1}{\sin^2 x}$$

$$= \frac{1}{v} \int \sin^v v x \, dv + \frac{1}{v} \int \frac{\cos v x \, dv}{\sin^v x}$$

$$u =$$

$$= - \frac{1}{v} \cot v x - \frac{1}{v \sin v x}$$

$$= - \frac{1}{v} \operatorname{at} v x - \frac{1}{v} \operatorname{ct} v x$$

$$\text{1. } y = \operatorname{arctan} \frac{u}{a}$$

$$du = \frac{a}{a^2 + u^2} du$$

$$\int \frac{du}{a^2 + u^2} = \frac{1}{2} \operatorname{arctan} \frac{u}{a}$$

$$\text{2. } \int \frac{du}{a^2 - u^2} = \operatorname{arsinh} \frac{u}{a}$$

$$\int \frac{du}{u^2 - a^2} = \int \frac{du}{u^2 - a^2}$$

$$\frac{1}{u^2 - a^2} = \frac{A}{u+a} + \frac{B}{u-a}$$

Want to find numerators

$$I = A(u-a) + B(u+a)$$

$$4 u = a$$

$$I = 2uB \quad B = \frac{1}{2}u$$

$$4 u = -a$$

$$I = -2uA \quad A = -\frac{1}{2}u$$

$$A = -\frac{1}{2}u$$

∴

$$C - \frac{1}{2}u \int \frac{du}{u+a} + \frac{1}{2}u \int \frac{du}{u-a}$$

$$= -\frac{1}{2}u \log(u+a) + \frac{1}{2}u \log(u-a)$$

$$= \frac{1}{2}u [\log(u+a) - \log(u-a)]$$

$$= \frac{1}{2}u \log \left(\frac{u+a}{u-a} \right)$$

$$\star \int \tan^{-1} dx = \int u^{n-1} du$$

$$\int \frac{du}{\sqrt{u^2 + a^2}}$$

$u = a \tan \theta$
use
 $du = a \sec^2 \theta d\theta$

Can integrate $\int \frac{\sin \theta du}{\sqrt{u^2 + a^2}}$

$$\int \frac{a \sec \theta d\theta}{\sqrt{a^2 \tan^2 \theta + a^2}}$$

$a \sec \theta$
 $+ a^2 \tan^2 \theta$

$$= \int \frac{a \sec \theta d\theta}{\sec \theta} =$$

$$\log(\sec \theta + \tan \theta)$$

$\sec \theta = a \tan \theta$
 $\tan \theta = a \sec \theta$

$$\int \frac{du}{u^v + u} = \log\left(\frac{u^v + u}{u}\right)$$

Known Prop ~~ac~~ ^{log}

Don't change sign under radical
because $= \sqrt{-1}$

$$\int \frac{du}{u^v - a^v}$$

$$u = a \sec \theta$$

$$du = a \sec \theta \tan \theta d\theta$$

$$= \int \frac{a \sec \theta \tan \theta d\theta}{a^v - a^v}$$

$$= \int \sec \theta d\theta = \log(\sec \theta + \tan \theta)$$

$$\frac{a^v \sec \theta}{\sqrt{a^v - a^v}}$$

$$\sqrt{a^v - a^v}$$

$$= \log\left(\frac{a^v \sec \theta}{a} + \frac{\sqrt{a^v - a^v}}{a}\right)$$

$$= \log(u + \sqrt{u^2 - a^2})$$

Q p ~ 0.5

$$\int \frac{dx}{\sqrt{x^2 + 1}}$$

$$= \frac{1}{2} \int \frac{u = \sqrt{y}}{\sqrt{y^2 + 1}} dy$$

P. p. ~ 0.5

even prob - ✓✓

p. ~ 0.7
odd prob to 17

6.6.5
202

$$\sim 1/\sqrt{6}/3 \sqrt{v}$$

$$\int \frac{\sqrt{v} \, dy}{\sqrt{x^v - 1}}$$

$$\text{let } x^v - 1 = u$$

$$du = v x^{v-1} dx$$

$$= \int u^{-\frac{1}{v}} du$$

$$\frac{(x^v - 1)^{-\frac{1}{v}}}{\frac{1}{v}} = v(x^v - 1)^{-\frac{1}{v}}$$

~~$\sqrt{v(x^v - 1)^{-\frac{1}{v}}} + \log(v + \sqrt{x^v - 1})$~~

next part

work to 18 p. $\log v^{1/10}$

Study ~~Time 153~~

work a little
 $\log v^{1/10}$

Integration by Parts
all over prob,

view

3/11/3v

$$\int \arctan x \, dx = x \arctan x - \frac{1}{\sqrt{1+x^2}}$$

$$u = \arctan x$$

$$du = \frac{dx}{1+x^2}$$

$$dx = \frac{du}{1+u^2}$$

$$= x \arctan x - \frac{1}{4} \log(1+u^2) + C$$

$$\int x^3 \arctan x \, dx = \int \arctan(x^4) \, dx$$

$$u = \arctan x^4$$

$$du = \frac{dx}{1+x^8}$$

$$dx = x^8 \, du$$

$$u = \frac{x^4}{4}$$

$$= \frac{x^4}{4} \arctan u - \frac{1}{4} \int \frac{x^8 \, dx}{1+u^2}$$

$$x^8 = (x^4+1)(x^4-1) + 1$$

$$= \frac{x^4}{4} \arctan x - \frac{1}{4} \left(\int (x^4 - 1) dx + \int \frac{dx}{1+x^2} \right)$$

$$= \frac{x^4}{4} \arctan x - \frac{x^3}{12} + \frac{1}{4} - \frac{\arctan x}{4}$$

Solve equation by Parts

$$\textcircled{1} \quad \int x^k \arctan x dx$$

arctan x
 arc sin
 arc cos
 arc cot
 arc sec

(x - dx = dv)

$$\textcircled{2} \quad \int e^{ax} x - dx = \int k^x x - dx$$

$$[(k = e^{ax}) \text{ by def of logarithm}]$$

$$k^x = e^{x \log k}$$

$$= \int e^{x \log k} x - dx$$

$$\int \underbrace{(\log x)^m}_{u} \underbrace{x^n dx}_{dv}$$

$$du = m(\log x)^{m-1} \frac{dx}{x} \quad (\text{differentiate } u)$$

$$dv = x^n dx \\ v = \frac{x^{n+1}}{n+1}$$

$$V^m (\log x)^m - \frac{m}{m+1} \int x^{n+1} (\log x)^{m-1} \frac{dx}{x}$$

$$I = \int (\log x)^m x^n dx$$

$$\log x = y$$

$$x = e^y$$

$$I = \int y^m e^{ny} e^y dy$$

6.6.5
6.7.3

$$I = \int e^{ax} x^m dx$$

$$\begin{cases} u = x^m; du = mx^{m-1} dx \\ dv = e^{ax} dx; v = \frac{e^{ax}}{a} \end{cases}$$

$$= x^m \cdot \frac{e^{ax}}{a} - \frac{m}{a} \int e^{ax} x^{m-1} dx$$

(3) $\log x \sim x^m$

(positive integers
if negative \rightarrow go)

$\int \frac{e^x}{x} dx$ (integration by parts
using help)

$$e^x = 1 + \frac{x}{1!} + \frac{x^2}{2!} + \frac{x^3}{3!} + \dots$$

substitute.

$$\int \frac{1 + x + \frac{x^2}{2} + \frac{x^3}{6} + \dots}{x} dx$$

p. 39 Table 12
Improved Technology
Coke
Cement - also due to larger +
more efficient units

Compared with other industries
C.R.E. has higher ratio

- 71 for 1919 for all industries
- II wages, salary & raw material
- 1970 for wage ratio = 46.8,
+ 5% for salaries.
- Wage ratio II for wage to N for
other products
- Material ratio - almost as
important as capital ratio.
- Oils fluctuate & it pays
to buy on a favorable market
and carry excess of raw materials
but not too great at its cost.
- Oils are time factor of industry
in high buying as a whole importer,

623
L 51-4307

2021-1613 (C)

SAC, Philadelphia

7/10/50

SA T. SCOTT MILLER, JR.

HARRY GOLD, sus.
ESPIONAGE - R

EXHIBIT 65-4307-1B-13 (12) (Exhibit 23)

On 6/22/50, GOLD advised that these cards are laboratory notes of BILL BOHOLL, an employee of ABRAHAM BROTHMAN, in connection with work on the methyl methacrylate molding powder process on which BROTHMAN was working.

TSM:HLP
65-4307

Methyl Methacrylate Molding Powder

U.S. 2,171,765 Sept. 5, 1940 (Röhm & Haas)

Ag. suspension of a finely divided
polymeric methacrylic ester and
an anti-MeMe at least 10 times
as great as that of polymer is
polymerized. Granular product.

(C.A. 34: 199)

Methyl Methacrylate

Fr. 847,879 June 20, 1939 du Pont
U.S. 2,161,461 June 6, 1939

MeMe or styrene, with catalyst, is emulsified in H₂O and passed in a continuous manner and in a turbulent flow through a curved tube which is heated at a temp. high enough to effect the polymerization when it passes the heated zone. Examples of emulsifying agents and

plasticizers (eg diethyl phthalate) grey

65-9-6
65-9-7

(CA.94: v858)

Methyl Methacrylate

3,784,879 June 10, 1970
U.S. 2,161,481 June 6, 1939 DuPont

Apparatus and process for preparing a dispersion of methacrylic emulsion flows in a state of turbulent agitation through a heated tube for a time sufficient to effect polymerization.

Equip. might be
CA-33: 7317 adapted for greater power

Example: MeMe Pure
water 1200
Sodium lauryl sulfate 15 dissolved in
BP 17 dissolved in water
H₂O₂ (30%) 33% in water

The mixture is passed through colloid
mill, and then through heated
tubes.

stable emulsion

Methyl Methacrylate

Molding Powder

(DuPont)

U.S. 2,244,707 June 10, 1941 L.P. Habbuch

A product suitable for molding is prepared by subjecting to polymerizing conditions a mixture containing methacrylic acid together with 2-70 times its quantity of Me Me.

(C.A. 35: 6075⁹)

Methyl Methacrylate

U.S. 2,133,757 Oct. 11, 1939 D.E. Stain (duPont)

Me₂Me polymerized in granular form by dispersing Me₂Me (5 parts) in water (25 parts) containing about 0.3 part of a gel-like resin obtained by polymerizing the product of the reaction bet Me₂Me and aqua NH₃, and subsequently polymerizing the dispersion while stirring.

Methyl Methacrylate

U.S. 2,117,371 May 17, 1938 R. Hill (ImpChem Ind.)

Products suitable for molding or for uniting sheets of glass are formed by polymerization of Me₂Me and at least one unsat'd polymerizable ester (e.g. vinyl acetate). (No emulsion - product pale yellow)

C.A. 32: 5111

Methyl Methacrylate

U.S. 2,121,839. June 28, 1938 D.F. Strain (duPont)

A fluffy powder prepared by dissolving mon. in H₂O-MeOH (not over 72% mon.) and precipitating polymer is precipitated in fuliginous form. Polymer is separated and monomer adhering to polymer is removed. Powder suitable for molding and for lacquers.

C.A. 33: 6366

Methyl Methacrylate

Molding Powder

Fr. 844.091 July 18, 1939 - Imperial Chem. Ind.

Granular dispersions prepared by heating at 80°C under agitation by using MeMe 30 parts, water 100 parts and 0.3 parts of the persulfates of Ca, Mg, Ba. Persulfates of Li, Na, K, and NH₄ produce stable emulsions.

Example 2:

Me Me mon. 30 parts
diethyl phthalate 70 -
Water 100 -
Li per sulfate 1 "

Stirred vigorously at 80°C. After 1/2 hr.
temp. rises to 90-95°

stable emulsion

Example 3:

Me Me 33 part
Water 66 -
Li per sulfate 0.7 -

spherical granules

Methyl Methacrylate

Brit 471,755 Sept. 9, 1937. du Pont

Granular polymer prep'd from MM by subjecting it to kneading operation at a sufficiently high to induce polymerization. Polymerization catalyst, fillers, plasticizers, modifying agent (e.g. hexane, H₂O, EtOH, MeOH). Example: MeMe polymerized with or without (1) BzO₂, (2) stearic acid, (3) BzO and

diethoxyethyl phthalate; and (3). α -ethoxy
(2) and (1)

See
C-6-5.

CA. 92:1362

Methyl Methacrylate

Molding Powder

Br. 437,784 Oct. 28, 1935 du Pont

The MMe is polymerized *in situ* in a mixture of H₂O and H₂O-miscible org. solvent, the amount of H₂O being substantially such that further addn. would ppt. monomer at the temp. of polymerization.

[CA 32 : P 2794]

Expt. 8

Example: Me₂ is introduced through one inlet and mix. of MeOH and H₂O through another inlet into a steam-jacketed kettle provided with a stirrer. The mixture is heated to 65°C. and samples taken to determine when appr. of polymer begins, when fresh Me₂ is introduced to preserve the correct compn. of reaction mixture. Polymer is separated and dried.

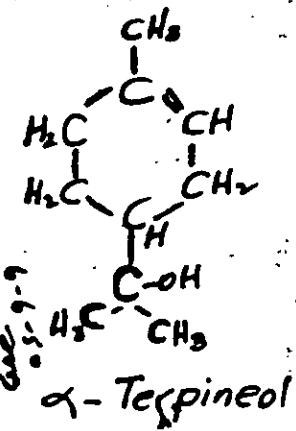
Methyl Methacrylate

Molding Powder

U.S. 2,701,395 May 21, 1955 D.A. Fletcher ^{DePont}

The molding material is prepared by mixing monomer with 3-14% its quantity of a α -terpineol and subjecting the mixt. to polymerization conditions.

(C.A. 34: 6365)



Colorless solid
m.p. ~~121~~ 38-40°C

Odor of lilac

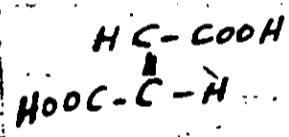
Methyl Methacrylate

Br. 548,717 Oct. 7, 1947 The British Thompson-Houston Co., ~~etc.~~

A water-sol. salt, for use as a granulating agent in prep'g synthetic resins fr. MeMe is prepared by subjecting to alk. hydrolysis polymerized alkyl ester of itaconic, fumare, mesaconic, citraconic or aconitic acids. (A.37: 6374)

$\text{HOOCCH}_2\text{C}=\overset{\text{C}}{\underset{\text{H}}{\text{C}}}.\text{OH}$ Itaconic Acid

CH_3



Fumaric Acid

MP 287°

S sol. in water

Aug. 9
05.00

✓ Methyl Methacrylate

Molding Powder

U.S. 2,765,247 Dec. 9, 1941 B. M. Marks (DuPont)

A granular polymer of MMe having adsorbed thereon a polymeric acrylic or alkyl acrylic acid is treated with an aq. soln of an alk phosphate, then washed with H₂O until free from salt.

(R.A. 36: 2046)

Methyl Methacrylate.

U.S. 2,796,403 Sept. 17, 1952 Renfrew & Gates
(Imp. Chem. Ind.)

MMA dispersed in an ag. vehicle,
in the presence of metal or alk. earth
metal persulfate, as a dispersing agent,
with more of the compound than that
which is soluble in the vehicle under
prevailing conditions.

(CA 37: 1211)

Methyl Methacrylate Molding Powder

U.S. 2,326,326 Aug. 10, 1943 J. Breedis (R.H.)

Moldable methacrylic resin prepared by injecting directly into water maintained at about 90-175°C, N_2O_2 through an orifice (0.5 mm. D) so as to cause the injected material to form as particles of such small cross section that they are heated

to the temp. of the water and
this polymerized in a few sec.

6-6-50
all

(CA.38: ✓99)

Methyl Methacrylate

Powder

Br. 395,687 July 17, 1933 R. Holl

Articles are manufactured by thermoplastic molding of product obtainable by polymerization in presence of diluent.

Elastomers: Camphor triethyl phosphate. Polymerization: (1) OP. \rightarrow 100°C
(2) AcOH & NaBQ₃. \rightarrow 60°C. (3) Mixing with titanium white & china clay

[CA 28: 5917]

See
05-6-919

Mark 50 Ge

Methyl Methacrylate

Ger. 735,784 Apr. 8, 1943 Rohm & Haas

mon. acrylates, methacrylates, and vinylates are mechanically emulsified without using emulsifiers, in an ag. suspension of powder substance inst. in the monomer or in H₂O. The emulsion is then polymerized.

(C.A. 38: 2770)

Fr. 844,073 July 16, 1939 I.G. Farben

Continuous polymerization of org. compds
in org. emulsions lighter than water
consists in using high liquid column,
introducing the org. compd and emulsion
liquid at the top, and evacuating
the dispersion of the polymerized products
through the bottom; the liquid being

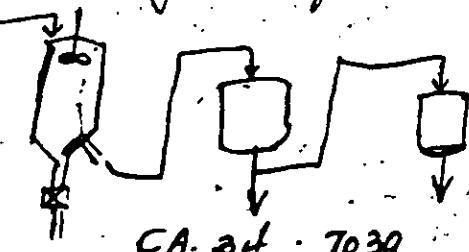
agitated only at the top.

monomer vinyl chloride

Emulsifying agent:

sod. d- oxy-octadecane

sod. persulfate



C.A. act : 7039

✓ U.S. 2,163,305 June 20, 1939 Harry R. Dittmer de Pont

methyl
A starch is used as a dispersing agent
in the polymerization of acrylic acid or
methacrylic acid or esters of these, and is
then removed, as by use of pancreatin
and HCl solution and washing. Procedure
given

C.A. 33: 7931

W.H. Sterck
OR Kreineler & R.W. Maxwell
Patent U.S.

etc.
1905

Soy with styrene gives a tougher article than with PVA.

Example 3: A mix of 25 part styrene, 1 part 50% and 100 parts of water were heated with stirring at 90-100°C under reflux for 24 hrs. Product washed with 60% alc. and dried.

Example 4: A mix of 15 part styrene, 65 parts methyl meth., 1 part 50% and 400 part water in a flask with reflux condenser & stirrer was heated with vigorous stirring under gentle reflux for 9 hrs. Some of the powder remained in suspension. Some acid was added to settle the suspension.

Styrene

Br. 511,417 Aug 18, 1939 duPont

Styrene, or a mix. of styrene and MeMe
is dispersed or dissolved in a liquid
medium is polymerized in the presence
of Sd as a catalyst.

CA 34: 1860

over

7
4 X 3.7
5-3
6

SAC, Philadelphia

7/10/50

SA T. SCOTT MILLER, JR.

HARRY GOLD, was.
ESPIONAGE - R

EXHIBIT 65-4307-1B-13 (13) (Exhibit 24)

On 6/22/50, GOLD stated that the name JAMES A. DEVLIN was that of an assistant in the laboratory at St. Joseph's College. GOLD stated that he was a day school student and was Father MALLEY's assistant and worked in the laboratory at night. GOLD stated that he met DEVLIN at the Franklin Institute and apparently DEVLIN had written his name and address on the back of a Franklin Institute call slip.

TSM:HKF
65-4307

James A. Devlin
6238 N. 4th St.,
Phila. 20,
Penn.

HA 4-1078

~~65-4302-1-B-13 (14)~~

Date Received

1/27/68

From

(Name of Donor)

(Address or Organization)

To

(Name of Recipient)

By

(Signature of Agent)

65-4307-10-313 (3)

6/6/50 Started 4:25 P.M.

65-4307

articles and items located and removed from
possession of Joe Gold 6823 Kindred St., Phila., Pa.

{ On fourth shelf of wooden cabinet in front
of basement

One hundred $8\frac{1}{2}'' \times 10\frac{1}{16}''$ sheets
of paper pertaining to answers to advertisements
for positions of employment giving Harry Gold's
background, education and experience in the
field of chemistry

Eight applications for Federal employment
U.S. Civil Service Commission requirement
for examination in field of chemistry
furnished by FBI

{ On fourth shelf of wooden cabinet
Eighty two $8\frac{1}{2}'' \times 11''$ sheets of paper
containing chemical formulae and notes on
experiments concerning lactide, butyl acetate
etc.
furnished by FBI

6/6/50

65-4307

On fourth shelf of wooden cabinet

Twenty two $8\frac{3}{8}'' \times 10\frac{5}{16}''$ sheets of paper containing chemical formulas and notations on experiments with also a white sheet of paper $7\frac{7}{8}'' \times 4\frac{5}{16}''$ attached to one of these yellow sheets. - On one of these yellow sheets the words are contained

On Lazaridis' method:

Zalkaova - See Reports Leningrad State Univ.

Seven $4\frac{5}{16}'' \times 7\frac{7}{8}''$ red sheets relating to "Lab. organization, Lab Work, monomer portions and pure monomer

Photostatic copy of U.S. Patent Office Document # 3,371,138 concerning granular polymerization of ethenoid monomers

Photostatic copy of document bearing number 4,44,257

relating to plastic material and methods of production

Photostatic copy of document bearing number 5,04,734

concerning improvements or relating to the manufacture of Methacrylic Acid Esters

Seven sheets of white paper $8\frac{1}{2}'' \times 11''$

pertaining to Nylon and containing chemical formulas
One $8\frac{1}{2}'' \times 11''$ sheet of gray paper containing chemical formulas

6-6-50

65-4307

(continuation of contents of Manila Folder 12 C)

One yellow sheet 8 $\frac{1}{2}$ " x 11" containing notation
"Tare & monomer"

Three yellow sheets of paper 7 $\frac{1}{2}$ " x 12 $\frac{1}{2}$ "
containing notation Nylon CA 1945 and
reflecting information concerning processes

Two white sheets of paper 4 $\frac{3}{4}$ " x 7 $\frac{15}{16}$ "
relating to chemical experimentation
found by DOD

On fourth shelf of wooden cabinet

Four sheets of white paper 8 $\frac{1}{2}$ " x 10 $\frac{15}{16}$ "

Three of which bore notation "Am OH - Hexine Run"
and the fourth sheet notation "Theory"

Letter or attorney of Amoco Chemical Co dated
7/16/47 addressed to Brothman & Associates
concerning submission of sample of Special Wax #1111

Leaflet of Durite Glass Apparatus Co, Inc., Bloomfield

N.J. re "The Improved Heating Jacket"

Brochure of Hendrick Mfg Co re "Hendrick
Mixing Equipment"

- 4 -

6-6-50

65-4307

(continuation of contents of Manila Folder 12 D)

Leaflet captioned "Precise Fractionation Assembly
Used by the National Bureau of Standards" distributed
by The Emil Gruner Co., N.Y.C.

Leaflet of The Emil Gruner Co., N.Y.C. re Carterion
Manostat.

Leaflet of The Emil Gruner Co., N.Y.C. re Stainless
Steel Weights

Pages 217 and 218 Chemical & Metallurgical Engineering
issue Jan. 1946 - Page 217 concerns Heat Transfer Equipment

Pages 219 and 220 Chemical & Metallurgical Engineering
issue Jan 1946 - Page 219 concerns General Chemical

Co - Supply List for American Industry
are white sheet of paper 8 1/2" x 11" with
notation "Conditions" and containing diagram
found by 373D

on fourth shelf of wooden cabinet
Thirty seven sheets of white paper 8 1/2" x 11"
which bears the date of Feb. March, April and May 1947

some of which are captioned "Esterification with P₂O₅"
and pertain to experimentation, list chemical processes
found by 373D

12 D
12 E

5

6-6-50

65-4307

for one month
of seven
days

In one month of value

One four sheet of wood cabinet
 Sixteen sheets of white paper $8\frac{7}{16}'' \times 10\frac{15}{16}''$
 captioned "apple 31 The Oxidation of Derivatives
 of Acetylenic Alcohols and Glycols"
 Thirteen sheets of white paper $8\frac{7}{16}'' \times 10\frac{15}{16}''$
 captioned "apple 21 The Oxidation of Acetylenic
 Alcohols and Glycols"
 Eleven sheets of white paper $8\frac{7}{16}'' \times 10\frac{15}{16}''$
 captioned "apple 6 Synthesis of Acrylic
 Monomers"

These pieces of papers were clippings together
 the sixteen sheets in one group, the thirteen
 in another group and the eleven in another group
 found by O'DD

-6-

6-6-50

65-4307

on fourth shelf of wooden cabinet

One two page letter dated 2/21/47 on the stationery
of Pennie, Edmonds, Morton and Barrow
Counselors at Law, N.Y.C addressed to Mr.
Abraham Brothman signs Arnold R Workman
referring to Brothman's patent date relating to
the process of manufacturing methyl
methacrylate monomer - On Page 2 it is
reflected that Russian literature citations were
not used against the Vaughn patent.

Letter dated 1/7/47 on the stationery of American
Cyanimid Co., N.Y.C addressed to A Brothman
and Associates signs E J Tuthill, Synthetic
Organic Chemists Dept. referring to Brothman's
interest in Ammonium Metavanadate, and
a shipment of the same.

A sheet of white paper $9\frac{1}{2}'' \times 10\frac{5}{16}''$
containing several numbers; the number
"0.453 x 454 = 206 grams" is at top of page

Three sheets of white paper with caption
"Linen 1"; "Let us offer" "Textured Paper Division"
found by JDD

6-6-50

65-4307

On fourth shelf of wooden cabinet

Three sheets of white paper $8\frac{1}{2}'' \times 11''$ with captions "Polymer on higher ketone solv-

- - thin streams distill Ketone,"

also "Particle shape," and "Surface Theory"

One white sheet of paper $8\frac{1}{2}'' \times 11''$

with inked notations - first line reads "Sample bottle full = 346.6 gms.

One white sheet of paper $4\frac{15}{16}'' \times 7\frac{5}{16}''$ -
first line reads "Dithylene Glycol monolaurate"
and word "Glaurin" appears on second line

Two sheets of white paper with captions

"Program for Typing Powder Work"
- much inked captions

I Removal of Adhered (?) Gum Arabic Film

II Use of Emulsifying Agents Requiring
Smaller Amounts than Gum Arabic

III Use of Diethyl Phthalate Polymer as a
Dispersing Agent

IV Emulsification in Alkaline Medium

6-6-50

-8-

6-6-50

65-4307

(Continuation of contents of Gravel Folder 12 I)

Reprints from India Rubber World, June 1944
of article entitled "Polymerization of
Vinyl derivatives in Suspension" by
W P Shoenstein, F Vingiello and H Mark
Polytechnic Institute of Brooklyn. This
article reprinted with compliments of The
Whitney Black Company, New Haven Conn.

Reprints from India Rubber World, January 1945
of article entitled "The Formation of Vinyl
Polymers in Emulsions and in Suspensions" by
S Siggia, W P Shoenstein and H Mark
Polytechnic Institute of Brooklyn

Photostatic copy of an from Industrial
and Engineering Chemistry Vol 37 no 4
April 1945 entitled "Emulsion Polymer-
ization of Acrylic Esters by W C Martz,
Lee Smith and C H Fisher, Eastern
Regional Research Laboratory, U.S. Department
of Agriculture, Philadelphia, Pa
including pages 366 through 369

6-6-50

65-4307

(Continuation of contents of Month Folder 12 I)

Seven sheets of white paper 8 $\frac{1}{2}$ " x 11"

containing inspection captions at top of page

U.S. 2,163,305 June 20, 1939 H. R. Dittmer (duPont)

U.S. 2,201,395 May 21, 1940 A. G. Fletcher (duPont)

U.S. 2,244,702 June 19, 1941 L. P. Habbush (duPont)

Br. 437,384 Oct 28, 1935 duPont

U.S. 2,265,242 H. Marks (duPont)

U.S. 2,133,257 Oct 11, 1939 D. E. Strain (duPont)

U.S. 2,171,765 Sept 5, 1940 Rohm + Haas

These relate respectively to

use of methyl or ethyl starch as emulsifying agent

mixture of methyl methacrylate and distilled water

" distilled water and methyl methacrylate

solutions prepared from methyl methacrylate, water and methanol

polymethacrylic acid as a granulating agent

solution of water soluble polymethacrylonitrile

colloidal suspension of aluminum hydroxide

Twenty sheet of yellow paper with pencil

writing and one blank piece of yellow paper 8 $\frac{1}{2}$ " x 11 $\frac{1}{8}$ "

some of these pages pertain to methylation of

-10-

6-6-50

65-4307

(continuation of contents of Manila Folder 12 I)

starch, ethoxy-methylene-malonic dinitrile,
ethyl-orthoformate, Liebig's Annalen der Chemie,
possible modification in vitamin synthesis,
Ribroplaxine, Vitamin C (L-ascorbic acid)

11 One sheet of white paper first line reads
"2,071,250 (rest numbers were not
completely discernible). This sheet 8 $\frac{1}{2}$ " x 11"

12 One sheet of yellow paper 8 $\frac{5}{16}$ " x 8 $\frac{1}{2}$ ".
dated 9/25/46 first line reads "Run

diethyl Phthalate Polymer for Reaction Time"
contains notation "Russian job - Carl Dyer".
One blank piece of paper 8 $\frac{5}{16}$ " x 10 $\frac{7}{8}$ "

Two sheets of white paper 8 $\frac{1}{2}$ " x 11"
captioned "a New Way of Using CaC₂"

White sheet of paper 8 $\frac{1}{2}$ " x 11"
with inked notation concerning metal
reflector in prism box of abbe refracto-
meter - signed Dr. W. Wayne

U.B. 9863 also on this sheet of paper
found by STB

6/6/50

65-4307

On fourth shelf of wooden cabinet

Two sheets of white paper containing pencilled
notations and one sheet of blank white paper

$8\frac{1}{2}'' \times 11''$ - one piece of paper has
caption "Illustration" - second piece
of paper contains notation which appears
to be $5\frac{1}{2}$ - 1 Hexine

Ten pieces of white paper $5\frac{1}{2}'' \times 8\frac{1}{2}''$
stapled together with stamped date
of Nov 29 1946 appearing on first page
and pencilled notation of date 12-3-46
and 12-3-46 on subsequent pages
notations on pages referring to Hexine
and Ketone possibly refers to
experiments

One piece of yellow paper $5\frac{1}{2}'' \times 8\frac{1}{2}''$
refers to mixture of Armac and HOH (water)

One piece of white paper $3\frac{5}{16}'' \times 5\frac{5}{16}''$
with diagrams of butane and acid

Four pieces of white paper $5\frac{1}{2}'' \times 8\frac{1}{2}''$
with notation on first page 12-6-46 and
"butane by Keggin's method" and

6-6-50

65-4307

(continued from content of Manila Folder 12-2)

dates 12/6 and 12/6/46 on succeeding pages
 nineteen sheets of white paper $5\frac{1}{2}'' \times 8\frac{1}{2}''$
 stapled together - pencilled notation of
 date on first page "12-5-46" and on some
 of succeeding pages and stamped date
 and pencilled date 12-16-46 on other pages -
 thirteen of above notation page blank
 six have pencilled notations appearing
 thereon - first page has notation w.t.
 of KOH, acetone, third page has
 notation hydrolysis of 1st fine.
 Nine sheets of white paper $5\frac{1}{2}'' \times 8\frac{1}{2}''$
 contain references ether solution, distillation
 and ether distillation - other sheets
 have dates of 12-23-46 and 12-26-46
 appearing at tops of some of the pages
 and cross notations C-23 + C-24
 Four sheets of white paper $4\frac{5}{16}'' \times 7\frac{5}{16}''$
 containing chemical formulas

13-

6-6-50

65-4307

(continuation of contents of Manila Folder 12-5)

Blank piece of paper ^{white} $8\frac{1}{16}'' \times 10\frac{15}{16}''$

One sheet of white paper " " "

Containing notations C 35-22 grm. 1946
on top line

One sheet of white paper $8\frac{1}{16}'' \times 8\frac{1}{16}''$

with mathematical equations and saturation
line "curve"

Three sheets of white paper $5\frac{1}{2}'' \times 8\frac{1}{2}''$

On first page notations 1) Absorber 3) Keggin
X Today's run 3) Binder - on second

page percentage figures are stamped date
Nov 27, 1946 appears - on third page

notations 29.7 coms KOH appear on fourth

sheet of white paper $5\frac{1}{2}'' \times 8\frac{1}{2}''$

eight of these pages are blank - pencilled
notations on other pages refer to methyl,
hydroxy, butine, acetone, butane synthesis
dates appearing at top of pages 12-9-46, 12-10-46

12-11-46, 12-12-46 - these pages stapled together

-14-

6-6-60

65-4307

(continuation of contents of Manila Folder 12-5)

Twenty three sheets of white paper $5\frac{1}{2}'' \times 8\frac{1}{2}''$
four of these sheets are blank - all twenty
three sheets stapled together - date appear-
ing at top of pages include 12-17-46, 12-8-46
and 12-20 - notation C-21 appears
at top of one page - references on these
pages to acetone, distillation

Seven sheet of white paper $8\frac{1}{2}'' \times 10\frac{15}{16}''$
with mathematical equations appearing thereon

Four sheets of yellow paper $8\frac{1}{2}'' \times 11''$

two of which have notation at top

"Class I" and "Class II" - these pages
refer to hexane and butane also to
oxidation of carbides to acetyllic acid
molecules

Two sheets of white paper $4\frac{15}{16}'' \times 7\frac{15}{16}''$

first page contains mathematical equation
second page refers to Acetone, Butane

Hexane

-15-

6-6-50

65-4307

(continuation of contents of sample folder 125)

One sheet of white paper 8 $\frac{1}{2}$ " x 10 $\frac{5}{16}$ " containing chemical formula - word "reaction at top" of left hand corner or one side of this sheet of paper - name "in density C 07-2119 at top of left hand corner reverse side of paper

One sheet of white paper 8 $\frac{1}{2}$ " x 11" notations may, Urbana, Brucklich, N E 9-2302 appear at top of page on one side - on reverse side at top left hand corner "A. Brothman" over one sheet of white paper 8 $\frac{1}{2}$ " x 10 $\frac{7}{16}$ " on stationery of A. Brothman and Associates - notation at top of page reports filtration on Buchner funnel with dry-ice acetone trap to vacuum line - at lower left of page "C 07-2119 after 1" or before 12" appears at lower left of page

One sheet of white paper 8 $\frac{1}{2}$ " x 11" containing chemical formulae

One sheet of white paper 8 $\frac{1}{2}$ " x 11" captioned "Experiment 1-7-47" relating to 270 g of methyl alcohol + 10 g KOH.

6-6-60

65-4307

(Continuation of contents of Manila folder 125)

One sheet of white paper dated 11-4-46

relating to experiment - page $8\frac{3}{8}'' \times 11''$

One sheet of white paper $8\frac{3}{8}'' \times 11''$ - first
line reads 25g monomer

One sheet of white paper $8\frac{1}{2}'' \times 10\frac{15}{16}''$ - first
line reads make set-up as per Expt. C 33

(urea trap for methylol). reverse side has
notation Call Mr Bronstein among 4-6520

One sheet of white paper $8\frac{3}{8}'' \times 11''$ containing
chemical formulas - on one side of page
ether extractions mentioned - on reverse side
notation appears 6th Ave + 42nd Bryan

1 P. A. Jewels 1095 6th Ave San Fran

Ten sheets of yellow paper clipped together
 $8\frac{3}{8}'' \times 10\frac{3}{16}''$ captioned & from Chem.

4 1347-52(1934) new method of applying
Calcium Carbide

Sixteen pages of white paper $8\frac{1}{2}'' \times 11''$ containing
chemical formulas

6-6-60

65-4307

(continuation of content of Manila folder 125)

5 Two sheet of white paper 8 1/2" x 11" - one sheet
has caption "Conference 3-11-43" and has
sub caption monomer synthesis powder
polymerization and sheet on bulk
polymerization - second sheet has
date 3-11-47 appearing on it and contains
chemical formulas

6 One white sheet of paper 4 5/16" x 7 5/16"
has notation at top 2155 R 11

1111-20 (1941)
found by 203

7 Found on fourth shelf of wooden cabinet
One sheet of white paper 8 1/16" x 10 5/16"
containing designs and chemical terms

8 Two sheet of white paper 8 1/2" x 11"
one sheet contains notation - titration methods
second sheet " " " " Manila Work
Tertiary Butyl Hydroperoxide

9 Table of four sheets of white paper - only
two white contain any writing - this consists of
numbers and chemical terms

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6-6-60

65-4307

(continuation of contents of Manila Folder 12K)

6-6-60
12K
12
One sheet of lined paper 8 1/2" x 11"
containing numbers and chemical terms
found by Agoy

Found on fourth shelf of wooden cabinet
Five sheets of white paper 8 1/2" x 11"
containing chemical formulas and notes
on experimentation

Two sheets of white paper referring to chemical
experimentation - these pages stapled together
Two sheets of white paper 4 15/16" x 7 5/16"
one page handwritten CA 29, 3926
same page " " *billet Kamchatka 1936 (9) 12*

Four sheets of white paper 8 1/2" x 11"
containing chemical formulas + experimental notes
Two sheet of white paper 8 1/2" x 11"
containing chemical formulas

Sheet of graph paper containing caption
solubility - GFW PER 1000 g H₂O

One sheet of white paper dated 6-9-47
captioned Vanishing Cream Formulas

6.6.50

65-4307

(Continuation of contents of Manila Folder 12-L)

Two sheets of paper of a Brothman and Associates - first page contains caption Scientific Glass - the first line

of second page begins "3 only # 5-732"

One sheet of paper with stamp of a Brothman and Associates relating to the

manufacture of Thioglycolic Acid (6-20-47)

One sheet of white paper 5 9/16" x 8 1/8"
captioned "VC Formulation"

One typewriter sheet dated 8-21-46

captioned The Preparation of Urea Form -
aldehyde cold - setting Glue

One sheet of paper of a Brothman & Associates

first line reads Satisfactory Monomerization
form by JOP

Found on first shelf of wooden cabinet

Three sheet of white paper dated

3-10-48 referring to Organolysis

of Dimethyl Isopropyl Ester and
Organolysis of methyl Butene

form by JOP

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6-6-50

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Found on fourth shelf of wooden cabinet
Monte Golden Barber Patent Literature
Search on Methyl Methacry.

One sheet of paper on a Brothman
and Associates stationery which is
captioned On the Monomer Synthesis
Three sheets of lined paper dated
7-25-46, 4-9-46, 4-15-46 and 4-24-46
These are captioned The Melting
Powder, Preparation of Pectin, Recrystalliza-
tion of Pectin from Acetone - last
page appears to be stereographic notes
Four sheet of paper slipped together
dated 5-2-47 captioned The Synthesis
of 2, 5-Dimethyl - 2, 5-Dihydroxy - Hexane 3
One white sheet of paper 8 $\frac{1}{2}$ " X 11"
middle of page contains notation See 668,870
See 12,1938 Walther Koch
One sheet of graph paper containing notation
diol, water, methylal

6

65-4307

6-6-60

(Continuation of contents of manila folder 12N)

Two typewriter papers containing sub-captions
methyl-butandone, vapor phase esterification,
methyl ester, chlorform, methoxy-isobutyric
acid, methyl methoxy-isobutyrate and
catalytic de-aldehydation - date Dec
19, 1946 appear at bottom of second page

In one
envelope
yellow
One sheet of yellow paper $8\frac{7}{16}'' \times 10\frac{5}{16}''$
containing chemical formulas
found by FBI

On further shelf of wooden cabinet

In one
envelope
white
One sheet of white paper captions
bold, W.t. of me me, for 86-850mm
and 10x tiny over four columns

One sheet of paper captions casting

One sheet of paper "Physical Test
Specimens"

One sheet of paper captioned $\frac{3}{16}$ " sheets
found by FBI

6-6-50

65-4307

Found on fourth shelf of wooden cabinet
one sheet of paper 8¹/₂" x 11" first
line of which reads 2,4 di chloro Benzaldehyde
- notation in middle of page on this sheet

4 A U.S. Tariff Comm Work o.c

Two sheets of paper dated 4-3-47
captioned UC relating to UC for
sun and wind burn
found by JHD

Found on fourth shelf of wooden cabinet
Two typewritten copies, three pages in length, of a
"Report of Plate Coating Tests in Modified R-21 Dope"
These copies were identical in content with the ex-
ception that the date Oct 3, 1932 appeared on one
copy but no date appeared on the other. Under
a sub caption "Discussion of Results" it was
reflected in the past year (possibly 1931) a
method had been found by which all methyl
alcohol soluble nitrocellulose could be made
with a yield which, in small experiments,

6-6-50

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(Continuation of contents in Manila Folder 12 A)
compare favorably with those obtained with
O.R. and R.P. types.

seven graphs captioned as follows

Electrometric Titration of 1.73% Kurlak Peck
Experimental Gelatin 50.366.

Electrometric Titration of 1.76% # 26707

Fresh sun calf skin Gelatin

Electrometric Titration of 1.74% # 1581

Acid-washed Acid Pig Skin Gelatin

Electrometric Titration of 1.70% # 17912

Acid-washed Pig skin Gelatin

Electrometric Titration of 1.73%

Bone Stock (Denitelle) gelatin

Electrometric Titration of 1.72% # 5351

Enriched Gelatin

Electrometric Titration of Stoves

Blended Gelatin # 1164

A two page document captioned: Method
of operating machine above the Upper

6-6-50 (Continuation of Contents of Minibinder 12Q) 65-4307

Explorim Limit, July 27, 1933, and signed
Harold W Brinck, Attached to this document was
a graph captioned: CO₂ - Acetone - air
Graph for Thermal Conductivity Cells, Cell
Jacket Temp. 98.8 - 99°C, Cell Current 280 M.A.

A two page copy of the minutes of meeting
discusses change to low viscosity Linters
for R. P. Cotton dated September 27, 1933.

The minutes were signed by E. K. Davis,
Department of Manufacturing Experiments.

A photostatic copy, four pages in length,
of report number V 1.185 captioned: Report
on Improved "Kodatrace" by R. Lendvai,
Vincennes Factory, dated March 21, 1935.

Kodak Pathé, Vincennes, France.
attached to this photostat was a diagram
captioned Installation Required for
Coating of improved Kodatrace.

A two page typewritten copy dated
November 25, 1935 captions Proposed Change
in Wind Up for Machine Located in Building 20.

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(Continuation of contents of Manila Folder 12A)

A six page typewriter copy captioned Chemical Plant, Kodak Pack, dated December 19, 1935, on the subject Analysis of solvent mixtures of Butyl Alcohol, Ethylene Dichloride, and Propylene Dichloride.

A three page typewriter document dated November 12, 1935, captioned Conference for discussion of Position vs Tendency Rights for R.C. Machines - November 12, 1935.

A two page typewriter copy of the minutes for a sub-conference dated November 29, 1935 signed G. J. Bebbcock

A three page typewriter document captioned The Sub Conference of October 3, 1936.

A two page typewriter document captioned Sub Conference of October 16, 1936

A two page typewriter document captioned Sub Conference of October 23, 1936

A two page typewriter document captioned Sub Conference of October 30, 1936

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(Continuation of contents of Manila Folder 12 G)

A two page typewritten document captioned
Sub-Conference November 6, 1936

A three page typewritten document captioned
Sub-Conference of November 13, 1936

A four page typewritten document captioned
Sub-Conference of November 20, 1936

A five page typewritten document captioned
Sub-Conference of November 27, 1936

Five page typewritten document captioned
Sub-Conference of December 4, 1936

Four page typewritten document captioned
Sub-Conference of December 11, 1936

Six page typewritten document captioned
Sub-Conference of December 18, 1936

Five page typewritten document captioned
Sub-Conference of January 8, 1937

Three page typewritten document captioned
Sub-Conference of January 15, 1937

Four page typewritten document captioned
Sub-Conference of January 22, 1937

6-6-50

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(Continuation of content of Manila Folder 12)

Manila Folder 12 Q	A five page typewritten document captioned Sub-Conference on February 5, 1937
	Four page typewritten item captioned Sub-Conference of February 12, 1937
	Four page typewritten document captioned Sub-Conference of February 19, 1937
	Four page typewritten document captioned Sub-Conference of February 26, 1937
	Three page typewritten item captioned Sub-Conference March 12, 1937
	Four page typewritten document captioned Sub-Conference of March 19, 1937
	Seven page typewritten document captioned Sub-Conference, Friday, April 2 or Tuesday April 6, 1937
	Four page typed document captioned Sub-Conference of April 9, 1937
	Five page typewritten document captioned Sub-Conference of April 16, 1937

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(continuation of contents of Manila folder 126)

Three page typewritten document captioned
Sub-Conference of April 23, 1937

Three page typewritten document captioned
Sub-Conference of May 7, 1937

Three page typewritten document captioned
Sub-Conference of May 14, 1937

Three page typewritten document captioned
Conference May 21, 1937

Three page typewritten document captioned
Sub-Conference May 28, 1937

Two page typewritten document captioned
Sub-Conference June 4, 1937

Two page typewritten document captioned
Sub-Conference June 11, 1937

Two page typewritten document captioned
Sub-Conference June 25, 1937

Five page typewritten document captioned
Status of Sub-Conference matters

August 31, 1937

6.6-50

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(Continuation of contents of main folder 12A)

Four page typewritten document captioned

Sub-Conference for September 10, 1937

Attached to this document was a page captioned

Amyg. brittleness Results on Safety X-ray
from 1934 to Present time.

Q

Three page typewritten document captioned

Sub-Conference of September 17, 1937

Four page typewritten document captioned

Sub-Conference of September 24, 1937

N

Three page typewritten document captioned

Sub-Conference of October 1, 1937

1

Three page typewritten document captioned

Sub-Conference of October 8, 1937

2

Three page typewritten document captioned

Sub-Conference of October 15, 1937

3

Three page typewritten document captioned

Sub-Conference of October 22, 1937

4

Three page typewritten document captioned

Sub-Conference of October 29, 1937

5

Two page typewritten document captioned

Sub-Conference of November 5, 1937

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(Continuation of contents of Manila folder 12Q)

Two page typewritten document captioned

Sub-Conference November 12, 1937

Two page typewritten document captioned

Sub-Conference November 19, 1937

Two page typewritten document captioned

Sub-Conference December 3, 1937

Three page typewritten document captioned

Sub-Conference December 10, 1937

Three page typewritten document captioned

Sub-Conference December 17, 1937

Four page typewritten document captioned

Sub-Conference December 31, 1937

Three page typewritten document captioned

Sub-Conference January 7, 1938

Three page typewritten document captioned

Sub-Conference January 14, 1938

Two page typewritten document captioned

Sub-Conference January 21, 1938

Three page typewritten document captioned

Sub-Conference January 28, 1938

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(Continuation of contents of Manila folder 12Q)

Five page typewritten document captioned

Six Conference February 4, 1938

Four page typewritten document captioned

Six Conference February 11, 1938

Four page typewritten document captioned

Six Conference February 18, 1938

Four page typewritten document captioned

Six Conference February 25, 1938

Four page typewritten document captioned

Six Conference March 4, 1938

Four page typewritten document captioned

Six Conference March 11, 1938

Four page typewritten document captioned

Six Conference April 1, 1938

found by 203

In all of the documents captioned

Six Conference on the various discussions

Trained later there were not - captions

dealing with chemicals and processes used
in photographic work and experiments

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paper no 122
of December 1950

Found on fourth shelf of wooden cabinet
Twenty eight sheet of white paper $8\frac{1}{2}'' \times 11''$
Only seven of them page contain writing -
first page contains standard solvent - it
and the succeeding pages contain chemical
formulas and mathematical equations
Found by ZBD

paper no 125
of December 1950

Found on fourth shelf of wooden cabinet
six sheets of yellow paper $8\frac{1}{2}'' \times 11''$
which contain chemical formulas and notes
on experiments - there are enclosed
in a manila folder, which bears notation
on outside "Notes from Doc"
found by ZBD

paper no 124
of December 1950

Found on fourth shelf of wooden cabinet
one sheet of white paper with caption Evaluation
of the new Unit for Absorbing CO_2
Blank sheet of white paper
Three typewritten pages concerning absorption
of CO_2 - one is very late date

6-6-50

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Four sheets of paper - three yellow and one white
clipped together - white page contains "Outline
of Rest." - first yellow sheet is
"Dinner Flotation Equipment" addressed to
see from Harry Gold and Joseph E. Brown

2nd yellow sheet contains table of results
3rd " " contains discussion of results

Four blank pieces of paper

Piece of white paper containing captions

Latent deposit unit, Turbo, Old Rest., dinner
Twenty nine yellow sheets relating to
tests and calculation concerning CO_2 -
none of them except one are blank

Pages 283, 286 & 307 of the May 1941 issue
of The Glass Doctor containing article
entitled "How to reduce the instability of
vitamin content" - a page & 3 is
signed by Ronald, Dougherty, Harry

Two typewritten sheets of paper dated 4/30/41

Captions Run #3 signed Harry Gold & Joseph
E. P. Brown

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{Continuation of Contents of Manila Folder 12T)

Forty eight sheets of yellow paper

One page captioned "Use of the Denver

Filteration Apparatus as an Absorber" -
result of several runs in 1941 reflected.

Typewriter sheet headed Harry Gold
June 30, 1938 captioned Recovery of
CO₂ from Other Gas

Nine typewriter sheets ^{four short} captioned "Use of
The Turbo - Mixer as an Absorber Unless
The Construction Cost of the Equipment
Per Pound of CO₂ Is Known"

Drawing containing some equipment
(possibly involving diffusion of gas through
water) is enclosed in drawing folder
containing this document captioned
"CO₂ Recovery"
dated 7-20-39

Found on fourth shelf of wooden cabinet
One white sheet of paper captioned
"Discussion 1. The War Job
on reverse side is notation Rpt #3
CO₂ Recovery

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(Continuation of contents of Manila Folder 12 U)

February 29, 1939 issue of the Industrial and Engineering
Chemistry News Edition

February 19, 1939 issue of the Industrial and Engineering
Chemistry News Edition

One sheet of white paper captioned note on CO_2
Recovery 142 with sub caption slate for
a 1 ton Plant

Eighteen sheets of yellow paper with caption
appearing at top Ethers, Acids, Lignins & materials
found by 23D

Found in fourth shelf of wooden cabinet
One hundred and forty miscellaneous sheets
of paper described as follows:

Thirty one sheets of paper on stationary of
a Brathman & Associates relating to the
subject Vanillin, Chloroform from CCl_4
and Standardization of Molding Powder Tests

- several of these sheets bear date in 1947
and have notation by 14 G

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65-4307

blue lined
Three sheets of white paper addressed
to Mr. Oser, one which sheet is signed Harry
and Phil, referring to the Stanton job
being in a precarious state and indicating
it would be impossible to develop a modi-
fication of the cyanohydrin process in a
few days so that Mr. Cole demonstrated
it in Switzerland

Eight pages of blue lined white paper
captioned Charge - then pertained
to lies concerning the Stanton job,
personnel problems concerning
Oser, Phil, Harry, Bill, Burnie
and Mankowitz

Sixteen blue lined yellow sheets
captioned Preparation of Substituted
Benzaldehydes

Eight pages of white paper dated
4-5-48 captioned Analytical methods
for Tests of 316 ELC "Standards"

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One two page letter on stationery of Julian Paul Brodie dated Sept 13, 1946 addressed by Julian P. Brodie to a Brathman refusing to agree to an agreement by Brathman's organization to develop men's vanishing cream with expenses for such work being borne by Brodie and listing the other terms of this agreement

7
6
5
4
3
2
1
0
-
1
2
3
4
5
6
7
8
9
0

Typewritten page captions "Program of Work For The Chinese Job" date 8/26/46 sixteen sheets of blue lined white paper some of which bear date of April 1948 containing chemical formulas, notes on experimentation and one sheet referring to specific jobs apparently being a Brathman & Associates

Twelve sheets of white paper some of which bear date in May 1947 containing experimental notes in chemistry

Three sheets of blue lined bright yellow paper one of which ^{and} contains chemical notations - the other two are written in French

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Exhibit 13
Exhibit 14
Exhibit 15

Three sheets of blue lined yellow paper
containing chemical experimental notes
Three sheets of red paper 3¹⁵/₁₆" X 6"
bearing diagrams and chemical symbols
- one of these sheets contains name of
Amson Corp 29 Bldg, N.Y.C and
the name of Mr Turner as prior to call
Twenty sheets of white paper 4" X 6"
containing chemical symbols and
notes on experiments
found by FBI

Found a portion of a wooden cabinet
One envelope postmarked Philadelphia,
Pa June 2, 1948 addressed Harry Gold
Elmhurst, N.Y.C having return address
on reverse side of envelope Mowell
& Doughty 5517 Litchfield St Phila
note enclosed in envelope from Alice
to Harry states "I hope you get
this in time see you soon"
found by FBI

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65-4307

3 small or fourth shelf of wooden cabinet
Budget Composition notebook - writing
first page of
one book refers to Patent of Jan 28, 1941

2, 229,897 American Cyanamid Co -
succinctly pages refer to Analysis of
Ozone, hydroxyisobutyric acid,
esterification of 2-OH isobutyric acid,
hexane synthesis - dates in this
book include Jan 23, 1946 to 3/25/47
- enclosed in this book were also eleven
sheets of blue lined yellow paper,
most of which bear date of September
1946, referring to chemical experimentation
found by JTD

16
Dec 16
1946

3 small or fourth shelf of wooden cabinet
Two page photostatic copy of U.S. Patent
Office Document # 2,030,901 concerning
Process for Depolymerizing Alpha Substituted
Acrylic Acid Esters
found by JTD

17
Dec 17
1946

3 small or fourth shelf of wooden cabinet
Two page photostatic copy of U.S. Patent
Office Document # 2,359,212 concerning
Process for Depolymerizing Polystyrene
found by JTD

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Found on front shelf of wooden cabinet
Federal Standard Stock Catalog L-P-406

Section IV part 5 - Federal Specification for
Plastics, Organic, General Specifications,
Test Methods - catalog date 1-24-44
found by JHD

Found on front shelf of wooden cabinet
Envelope postmarked N.Y.C. Nov 25, 1947

addressed to A Brantham and Associates
Long Island City, N.Y. bearing return
address The Cooper Alloy Foundry
Co., Hillside, N.J. - enclosed
in envelope was twenty one page
document captioned Memorandum
on the Preparation of Thio-glycolic
Acid Patent Papers

found by JHD

Found on front shelf of wooden cabinet
Envelope postmarked Dec 3, 1947 Louisville

Ky addressed to A Brantham and Associates
Elmhurst, Long Island bearing return
address The Girdle Corp., Louisville, Ky.
- enclosed in envelope were eight pieces

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of white paper bearing date of November
1946 referring to chemical experiments
such as synthesis and degradation of
acetylene - Glycols, Hydrogenation
of acetylene - Hydrocarbons, reaction
between Oz and acetylene in the
presence of Nitrogen oxide, oxalic
acid from acetylene etc. - also
enclosed in above envelope was
letter dated 12/3/47 from G E Blauth
Vice President of the Girdler Corp
submitting several circulars and pieces
of literature describing the Volator
principle of heat transfer and
processing and illustrating several
models of Volator units
(these enclosures still attached to
letter)

also enclosed was Gold Model Writing
Tobler Book bearing name of Harry Gold

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6-6-50

15-4307

- In this notebook are two pages dated
3-5-48 - one of the pages has as its
first line "OsO₄ Ref. Mellor XI p 707"
and in middle of this page is notation
"1. OsO₄ acts to influence rate of decompr.
of alkali chlorates"
- In second group do as at first line
"MoO₃ mellor XI p 545"
- Also in this notebook are four pages
dated 4-20-47
 - first page, first line reads "Bull.
de la Société Chimique 25, 346-369
(1901) and has subcaption "Formal-
+ Decomps. of Acetals -
 - second page, first line reads "Methylac-
+ 128 H₂O @ 14-26 °C
 - third page, first line reads "J. Phys.
Chim. 36, 2325-2337 and has
subcaption Decomposition of Methylac-
 - in this page

6-6-50

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front page, first line reads Berichte 70,
1713-1719 (1937) and has no caption

Hydrolysis of Acetal

five page, first line reads Berichte 67,
424-429 (1934) and has no caption

Velocity of Acetal Hydrolysis

(all other pages of this notebook are blank)

Inside inside of this notebook is a
piece of stationery of C. Böttger &
Associate - in upper left hand
corner is the date 11-2-47 and
written "14-6" - beside the caption
dot is the name writer and beside
the caption subject is the writing

C. (C.L.) 2 Process. in the body

of this piece of stationery are

the captions German, Mathison, Clinton

and in a single copy envelope are two

pieces of yellow paper $4\frac{1}{2} \times 5\frac{1}{2}$ ", one which
is blank, and the other which has a few thin
writing lines, use excess $\text{Fe}(\text{SO}_4)_3$ + add
 H_2O_2 slowly found by 200

Decay of Ethyl Carbonyl

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6-6-50

65-4307

Found on fourth shelf of wooden cabinet
Envoy postmarked Oct 29 1946 Philadelphia Pa
addressed Harry Gold, Elmhurst, L.I., N.Y.
bearing return address Ackerson Colloids
Corp., Philadelphia Pa.

Note on stationery of Ackerson Colloids
Corp Port Huron, Mich addressed
to Harry Gold on back which reads
"Wish you luck - see you on the week-
end" - reverse side has chemist notation
Sheet of white paper 8 1/2" x 10 15/16", first
line reads "1 Variable Take-off Still Head"
Sheet of white paper 8 1/2" x 10 5/16", first
line for notation V.F. Powd

Sheet of white paper 8 1/2" x 11", first
line reads "Solubility of p. Sulfuric Zincate 4"
with date 4-12-47 in upper right hand corner
One sheet of notebook paper 3 1/2" x 5 7/8"
first line reads "1. Vapor phase sterilization
found by 232

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6-6-50

65-4307

Found on first shelf of wooden cabinet
Forty small sheets of loose leaf paper
containing some punch holes and bearing
perforated notations which pertain to
industries, chemical processes, inventions
and patents and German language notes
(This may be school note since some
are dated in 1932 and bear two tabs
"Chem 107 and Gen 2")

found by J.H.J.

Found on second shelf of wooden cabinet
Twenty 3" x 5" index cards - seventeen
of which pertain to Methyl Methacrylate
- molding powder with specification
and uses for this same. of the
three remaining cards, one is captioned
Styrene and the other two ^{contain} notations
concerning the use of methyl starch
as a dispersing agent and the continuous

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6.6.60

65-4307

{ polymerization of org. compds in emulsion
{ found by JMB

{ Found on underside of wood cabinet
{ on $3\frac{1}{8}$ " x 6" piece of white paper
containing following writing done
a Devlin 6238 N. 4th St Phila
20 Penna 14 A 4-1078
found by JMB

Search discontinued at 6:00 P.M.

JMB